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2. 0207530.7 — 2 APR 2002

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THE UNIVERSITY OF NOTTINGHAM
UNIVERSITY PARK
NOTTINGHAM
NG7 2RD

Patents ADP number *(if you know it)* — 437692 7002

If the applicant is a corporate body, give the country/state of its incorporation — GREAT BRITAIN

4. Title of the invention

HIGH FIELD STRENGTH MICROWAVE PRODUCTION, AND MICROWAVE PROCESSING OF MATERIALS E.G. WEAKENING OF MULTI-PHASE MATERIALS

5. Name of your agent *(if you have one)* — Barker Brettell

"Address for service" in the United Kingdom to which all correspondence should be sent *(including the postcode)*

138 Hagley Road
Edgbaston
Birmingham
B16 9PW

Patents ADP number *(if you know it)* — 7442494002

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11. I/We request the grant of a patent on the basis of this application.

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Barker Brettell

Date 28.03.02

12. Name and daytime telephone number of person to contact in the United Kingdom — Mr. John Lawrence — Tel: 0121 456 1364

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DUPLICATE

HIGH FIELD STRENGTH MICROWAVE PRODUCTION, AND MICROWAVE PROCESSING OF MATERIALS E.G WEAKENING OF MULTI-PHASE MATERIALS

This invention relates to the production of high electric field strength microwave radiation, typically but not necessarily for the weakening of multi-phase materials using microwaves.

The invention arises from a consideration of how to process mined ores and it is convenient to illustrate it in that context. It will be realised that the invention has wider applications.

It is known to process, e.g. by milling, ores to extract a wanted mineral from unwanted surrounding rocks or minerals, comminution of ores is a well-established industry. Milling or grinding ores is very energy intensive. It has been estimated that one and a half percent of all energy used in the United States is used in the comminution of ores and minerals. It is very big business.

There are many suggestions as to how to pre-treat materials before they are processed by a milling/grinding machine. Some involve chemical treatment, some involve heat treatment, and there are proposals, but as yet unsuccessfully implemented, to pre-treat with microwaves. There is also a proposal to use electric discharges.

Some literature in the field includes:- United States Patent No. 5 824 1533, PCT Patent Application WO 92/18249, British Patent Application No. GB 2 120 579, and the papers "The Influence of Minerology on Microwave Assisted Grinding", S.W. Kingdom, W. Vorster and N.A. Rowson, Mineral Engineering Vol. 13, No. 2, Elsevier Science Limited, 0892-6875(99)00010-8; "Effects of Microwave

Radiation upon the Mineralogy and Magnetic Processing of a Massive Norwegian Ilmenite Ore" by S.W. Kingman, G.M. Corfield and N.A. Rowson, Magnetic and Electrical Separation, Vol. 9. published by Overseas Publishers Association N.V.; "The Effects of Microwave Radiation on the Processing of Palabora Copper Ore" by S.W. Kingman, W. Vorster and N.A. Rowson, published by The Journal of the South African Institute of Mining and Metallurgy, May/June 2000; "Microwave Treatment of Minerals – A Review", by S.W. Kingman and N.A. Rowson, published by Minerals Engineering, Vol 11, Elsevier Science Limited, 0892-6875(98)00094-6; "The Effect of Microwave Radiation on the Processing of Neves Corvo Copper Ore" by W. Vorster, N.A. Roswon and S.W. Kingman, International Journal of Mineral Processing 63(2001)29-44 published by Elsevier Science B.V.; "Short-Pulse Microwave Treatment of Disseminated Sulfide Ores" by J.B. Salsman, R.L. Williamson, W.K. Tolley and D.A. Rice, Minerals Engineering, Vol. 9, No. 1, 1996 published by Elsevier Science Limited 0892-6875(95)00130-1; "The Effect of Microwave Radiation on the Magnetic Properties of Minerals" by S.W. Kingman and N.A. Rowson, Journal of Microwave Power and Electromagnetic Energy Vol 35, No. 3, 2000; "Applications of Microwave Radiation to Enhance Performance of Mineral Separation Processes" by S.W. Kingman, N.A. Rowson and S. Blackburn, IMN 1997 ISBN-1870706388.

These discuss having conventional multi-mode microwave producing machines applying microwaves for quite long periods (10 seconds or much longer) to batches of minerals, and then processing them by crushing and/or grinding.

It is reported in the above papers that the energy expended in microwaving minerals can be far more than the energy saved in the comminution process.

The above means that in practice a designer of a mineral processing plant does not consider microwave pre-treatment as being at all feasible/desirable. It does not work in a way so as to reduce overall costs. There is a prejudice in the art away from using microwaves. It is not known that there is even a single production-scale facility that uses pre-treatment by microwaves as a conditioning step in the treatment of ores prior to comminution.

According to a first aspect of the invention we provide a method of rapidly heating a material comprising creating a standing wave of microwaves and a region of maximum electric field strength, and having material disposed in said region of maximum electric field strength.

We have realised that standard multi-mode microwave cavities, similar to those found in conventional kitchen microwave ovens, have many advantages, are very commonly available and are the equipment of choice for very many areas, but that they are not the best for some purposes where maximum electric field strength is required. Multi-mode cavities do not have a standing wave created in them – they deliberately "smear" their energy out uniformly across the cavity (or more or less uniformly) so as to achieve any effect evenly – or more evenly – throughout the volume of the cavity. This has been the drive of multi-mode cavity designers. However, we have appreciated that there can be times when processing a material when very high electric field strengths are required and that the best way to obtain these is to use a microwave cavity which can sustain, and does sustain, a standing wave. This standing wave then has maximum and minimum power density regions, which coincide with maximum and minimum electric field strength regions (there is a relationship between power density and electric field strength and electric field strength varies with a power greater than 1 in comparison to power

density - generally a squared power relationship). We have then appreciated that in order to apply the maximum electric field strength, produced by a typical microwave generator (or any particular specific microwave generator) it is desirable to align the position of the material to be processed with the position of the maxima in the standing wave. This can typically be achieved by controlling the position of the material relative to the cavity, but alternatively it is possible theoretically to move the position of the maxima to suit the position of the material within the cavity, by appropriately tuning the standing wave.

Preferably a single mode microwave cavity is used. A single mode microwave cavity enables us to provide a good standing wave.

A very important application of the invention is mineral processing to weaken the bond between a first phase of material and a second phase of material in a multi-phase composite material. For example, ores or minerals that are desired to be extracted are found in a different phase of rock.

By using microwaves to heat two phases in a material (e.g. rock) differentially it is possible to have differential expansion over the two phases, and to cause cracks or weakening of their interface. This can facilitate the extraction of the mineral from the rock. There is preferably still mechanical pre-treatment of the ore or rock to separate the first and second phase materials.

We have also discovered a very interesting, commercially useful, effect. It is necessary to heat multi-phase materials (or other materials) with microwaves using the standing wave technique for far less time than is previously been thought desirable. We may expose the material to high intensity microwaves first for something of the order of a second or less,

or the order of a quarter of second less, or the order of 0.1 of a second or less, or possibly even the order of 0.01 second or less. Depending upon the choice of first and second phase materials, about 0.2 of a second may be the best weakening effect for power expenditure with a power density appropriately high. Typical power density that we would have in mind might be about 10^{12} watts per cubic metre or above.

We have also appreciated that it is possible to pass material through a microwave cavity in a continuous stream, for a continuous treatment process. The microwave cavity has its standing wave in being and material can be made to move through the standing wave, residing in the high intensity region of the standing wave for only a short time. This has the double benefit of increasing the throughput of materials through the treatment machine, and using the knowledge that we do not need to apply microwaves to materials for very long to achieve the desired effect. The two advantages have synergistic effect.

According to a second aspect of the invention we provide a method of weakening the bond between a first phase of material and a second phase of material in a multi-phase composite material, the method comprising inducing a high thermal gradient at an interface between the first and second phases by applying microwaves with a power density of at least 10^9 watts per cubic metre, and creating a standing wave having an area of high electric field strength and positioning the material at or about the area of high electric field strength.

According to a third aspect of the invention we provide a method of weakening the bond between a first phase of material and a second phase of material in a multi-phase composite material comprising applying a high powered density of microwave, or high electric field strength

microwaves, to the composite material for an exposure time that is of the order of 1 second or less.

According to a fourth aspect of the invention we provide a method of microwave processing material comprising applying a high power density microwave, or high electric field strength microwave, to the material for an exposure time that is of the order or 1 second or less.

According to fifth aspect of the invention we provide apparatus for processing a material comprising a microwave cavity adapted to apply high power density microwaves to the material for an exposure time that is of the order of 1 second or less.

Preferably the exposure time is achieved by passing the material through the microwave cavity at a speed so as to achieve the desired exposure time.

According to another aspect of the invention we provide apparatus for weakening the bond strength between a first phase of material and a second phase of material in a multi-phase composite material comprising a microwave cavity adapted to apply high power density microwaves to the composite material for an exposure time that is of the order of 1 second or less.

According to another aspect of the invention we provide a method of continuous processing of ores or rocks comprising applying high power density microwaves, or high electric field strength microwaves, on a continuous basis to ore or rocks passing through a microwave cavity to weaken the ore or rocks, and subsequently passing the continuous flow of ore or rocks to a mechanical treatment machine and mechanically breaking up the ores or rocks.

We have found that we can achieve a reduction in overall energy consumption - quite a serious reduction - if we pre-treat the ore or rocks with microwaves so as to weaken them and then break them up in a mechanical comminution process.

Moreover, continuous process has a higher throughput, and can cope with higher volumes than batch processes. This makes the process even more economically attractive.

It is particularly elegant that once we have a high enough electric field strength (achieved by positioning the material at a maximum of a standing wave) we can then flow material (whether that be for weakening the bond between different phases, or other purposes) through the maxima in a continuous manner at a rate that is fast enough to expose the material to the high intensity microwave for only a short time, the fact that the material is exposed for a short time reduces the cost per unit of material, the fact that there is a continuous process improves the throughput, the fact that the materials have to flow quite fast through the microwave cavity improves the throughput, and all of these things reduce the cost of the processing per unit of material process.

According to another aspect of the invention we provide apparatus for continuous processing or ore or rocks comprising means for applying high power density microwaves, or high or maximised electric field strength microwaves, on a continuous basis to ore or rocks passing through a microwave cavity to weaken the ore or rocks, and feed means adapted to pass subsequently with continuous flow of ores or rocks to a mechanical treatment machine adapted mechanically to break up the ore or rocks.

We have appreciated that a higher temperature gradient is needed to separate ores and minerals from the surrounded unwanted material.

According to further aspects of the invention we provide a method of weakening the interface between a first phase of material and a second phase of material comprising creating a temperature gradient at an interface between the first and second phases of at least 100°C by using a standing wave of microwaves to heat the first and second phases differentially.

According to another aspect of the invention we provide apparatus for weakening the interface between, or separating, a first phase of material from a second phase material, the apparatus being capable of creating a temperature gradient at an interface between the first and second phases of at least 100°C by creating a standing wave of microwaves to heat the first and second phases differentially.

A single mode cavity may be provided to produce a standing wave.

Embodiments of the invention will now be described by way of example only, with reference to the accompanying drawings, of which:-

Figure 1a schematically illustrates a two-phase rock having crystals of a first material embedded in a second material;

Figure 1b shows schematically the rock of Figure 1a after treatment by microwaves according to the present invention;

Figure 2 shows schematically a mineral extraction plant and process in accordance with the present invention;

Figure 3A shows schematically a microwave pre-treatment unit for use in the apparatus of Figure 2;

Figure 3B shows how electric field varies across the material inlet of the unit of Figure 3A;

Figure 4 shows a variation of the unit of Figure 3A;

Figure 5 schematically illustrates a model of a calcite and pyrite ore sample;

Figure 6 illustrates dielectric loss factor versus temperature;

Figure 7 illustrates variation of microwave power density versus temperature;

Figure 8 illustrates the direction of simulated loading in a uniaxial compression test;

Figure 9 illustrates temperature distributions of a 2.45GHz, 2.6kW microwave cavity;

Figure 10 illustrates the effect of varying heating times;

Figure 11 illustrates the effect of microwave heating time on unconfined compressive strength;

Figure 12 illustrates shear plain development during unconfined compressive tests;

Figure 13 illustrates temperature distribution for a microwave cavity with a power density of 10^{11} W per cubic metre;

Figure 14 illustrates stress versus strain curves for different heating times;

Figure 15 illustrates unconfined compressive strength versus heating time for a power density of 10^{11} W per cubic metre;

Figure 16 illustrates shear plain development during unconfined compressive tests for power density of 10^{11} W per cubic metre;

Figure 17 illustrates point of load index versus heating time for a power density of 10^{11} W per cubic metre;

Figure 18 illustrates point of load index versus heating time for different power densities;

Figure 19 illustrates t10 versus ECS;

Table 1 shows specific heat capacity as a function of temperature;

Table 2 shows thermal conductivity as a function of temperature;

Table 3 shows thermal expansion co-efficient as a function of temperature;

Table 4 shows mechanical properties of different minerals;

Table 5 shows the effect of different heating times on temperature and compressive strength of material;

Table 6 shows similar factors to Table 5, but for a higher power density;

Table 7 illustrates breakage parameters for a multimode cavity power density between 3 x 10^9 W per cubic metre and 9 x 10^9 W per cubic metre;

Table 8 shows breakage parameters for a single mode microwave cavity with a higher power density; and

Table 9 is a list of references referred to.

Figure 1a shows rock material 10 comprising crystals 12 of a first material embedded in a matrix 14 of a second material. An example of the first and second materials might be metal oxides (e.g. magnetite, ilmenite or haematite), or metal sulphides (e.g. copper, iron, nickel, zinc, or lead) as the first material, and possibly silicates, feldspars, or calcite as the second materials. It will be appreciated that these examples are non-binding and are illustrative only. There could be third, or fourth, or subsequent, materials 16 also present in the rock material 10. Thus, the rock material 10 comprises multiple phases of material having grain boundaries 18 between them.

Figure 1b shows the rock material 10 after it has been treated with microwaves in accordance with the present invention. The crystals, or regions, of the first material 12 now have a weaker bond to the material 14, because the grain boundaries have been weakened due to the presence of cracks/dislocations/areas of stress and strain. These are referenced 20. In addition, there are also cracks 22 within the first material regions 12 and cracks 24 in the second material 14.

The precise nature of grain boundaries between two mineral phases in rock is not well understood, but it is suggested to be an area of disorder between two ordered species. If this were the case, then it would be sensible to assume that grain boundaries are an area of weakness. However, products of comminution suggest that grain boundaries are an area of strength (transgranular fracture being common in mineral processing operations) and can adversely influence liberation of one species from another. Thus, whilst theory might say that grain boundaries should be an area of weakness, practice in traditional comminution suggest that grain boundaries are particularly strong. However, it has been postulated that if microwave energy can induce micro-cracking around grain boundaries then reductions in required comminution energy and enhanced liberation of a valuable mineral would occur.

The reason why it is expected that cracks would occur at the grain boundary is due to the differential heating of the two material phases. They are expected to absorb energy from microwave differentially, and to change temperature at different rates, inducing thermal stresses. However, to date this has not really happened economically.

With the present invention, it has been realised that the reason why this has not happened is due to the temperature gradient not being large enough between the different phases of material. We have realised that to obtain a greater temperature gradient we should use a higher electric field strength/power density. The sort of power density we have in mind is perhaps of the order of 10^{15} Wm^{-3}, or 10^{14} Wm^{-3}, or 10^{14} Wm^{-3} (for example) for some applications. Depending upon the cavity design and dielectric of the material we may be generating electric fields of the order of 10^5 Vm^{-1} to 10^7 Vm^{-1}, perhaps in the range of 0.05×10^6 Vm^{-1}. These

figures are of course exemplary only and are non-binding and are not intended to be restrictive.

Numerical modelling has been undertaken using the geomechanical 2-D finite difference modelling software application, FLAC V3.3 (Itasca 1995). The model domain consisted an area representing a 15mm wide by 30 mm high section, which was subdivided into individual square zones of 0.04mm sides. The positions of the pyrite particles within the model domain were randomly generated to provide a relatively disseminated ore body, see Figure 5. This type of dissemination has previously been shown to be responsive to microwave heating. It is appreciated that the 'mineralogy' or texture used for the modelling may be a simplified version of reality. However, the purpose of the investigation is to determine the influence of power density on the degree of strength reduction, not mineralogy. Therefore, as long as the mineralogy or texture is the same for both tests the data can be truly comparative. What is important, however, is that the simulated ore contains species that are both responsive and non responsive to microwave heating.

The finite difference modelling comprised of the 5 main stages given below and more fully described later:

1. Microwave heating of the two different mineral phases
2. Transient heat conduction during heating process between minerals
3. Determination of peak thermally induced stresses and strains
4. Modelling of thermal damage associated with material failure and strain softening
5. Simulation of uniaxial compressive strength tests to evaluate the reduction of unconfined compressive strength due to microwave heating.

Stage 1: Microwave heating

The amount of thermal energy deposited into a material due to microwave heating (power absorption density) is dependent on the internal electric field strength, the frequency of the microwave radiation, and on the dielectric properties of the material

The power absorption density per unit volume of the mineral can be approximated from Equation 1.

$$P_d = 2.\pi.f.\varepsilon_o.\varepsilon''_r.E_o^2 \qquad (1)$$

Where
P_d is the power density (watts/m^3)
f is the frequency of the microwave radiation (Hertz)
ε_o is the permitivity of free space (8.854×10^{-12} F/m)
ε''_r is the dielectric loss factor of the mineral
E_o is the magnitude of the electric field portion of the microwave radiation (volts/m)

Because the microwave absorption factor for calcite is substantially lower that that for pyrite no microwave heating of the calcite matrix was assumed during the modelling with selective heating of the pyrite particles only. The early work of Chen. (1984) and Harrison (1997) shows this assumption to be realistic.

The dielectric loss factor, ε''_r, for pyrite has been found to be dependant on temperature (Salsman 1995). In determining the power density for the pyrite the relationship between ε''_r and temperature as shown in Figure 6 was utilised (Salsman 1995).

For an initial series of models the power densities at various temperatures was obtained for the heating of pyrite within a 2.6 kW, 2.45 GHz multimode microwave cavity. The calculated power density varied between 3×10^9 watts/m^3 at 300 °K and 9×10^9 watts/m^3 for temperatures greater than 600°K (Figure 7) (Kingman 1998). The initial temperature of the ore body sample was taken to be 300°K.

Stage 2 Modelling of Transient Heat Conduction During Microwave Heating

The transient conduction of the microwave thermal energy during heating was modelled using an explicit finite difference method written as an algorithm.

The basic concept in the thermal conduction modelling was that a thermal energy flux may occur between a zone and its four immediately adjacent zones. The direction, i.e. into or out of the zone, and the magnitude of the thermal energy flux was dependent on the temperature gradient that existed between the zones and the conductivity of the zone. The boundary conditions were such that no thermal energy was lost from the material i.e. the material was assumed to be fully insulated.

The basic law that was used to determine the thermal energy flow between the zones was Fourier's law, which has been given as Equation 2:-

$$q = K.T_{diff} \qquad (2)$$

Where q is the heat flux vector in joules/sec/m

K is the thermal conductivity tensor in w/m.°C

$T_{(diff)}$ is the temperature difference (°C)

Thus the change in stored energy per time increment, Δt, is given by Equation 3

$$.\Delta\bar{\beta} = \Delta t.p \tag{3}$$

$\Delta\beta = \Delta\delta q$ Where Δβ is the change in stored energy (Joules)

Expressing this in an explicit finite difference form for a square zone *i,j* with side length *l*:

$$\Delta\beta_{(i,j)} = \Delta t.K_{(i,j)} l \left[(T_{(i,j)} - T_{(i,j-1)}) + (T_{(i,j)} - T_{(i,j+1)}) + (T_{(i,j)} - T_{(i+1,j)}) + (T_{(i,j)} - T_{(i-1,j)}) \right] \tag{4}$$

Where $K_{(i,j)}$ is the thermal conductivity of zone i,j

Δt is the time increment in seconds

l is the length of the sides of the zones

$T_{(i,j)}$ is the temperature of zone i,j

The relationship between thermal energy in joules and temperature in °K for a given time increment, Δt, is given by Equation 5:-

$$\Delta T_{(i,j)} = \frac{\Delta\beta_{(i,j)}}{m_{(i,j)}.C_{(i,j)}} \tag{5}$$

where ΔT(i,j) = temperature change in zone i,j (°K)

m(i,j) = mass of zone i,j (Kg)

C(i,j) = specific heat of zone i,j (joules/Kg.K)

Thus at the end of each time increment the new temperatures of each zone due to thermal conduction and microwave heating are determined using Equation 6

$$T_{(i,j)}(1) = 300°K \quad T_{(i,j)}(n+1) = T_{(i,j)}(n) + \Delta T_{(i,j)} + Pd_{(i,j)}/(C_{(i,j)}.\Delta t) \tag{6}$$

Where $T_{(i,j)}(n)$ is the temperature of zone i,j at time increment n

$Pd_{(i,j)}$ is the power density of zone i,j

The microwave heating and thermal conduction for a specified heating time, ht, was simulated by recursively iterating Equations 4, 5 and 6 until Equation 7 was satisfied.

$$ht = n.\ \Delta t \tag{7}$$

Where: n time increment number

Δt is the time increment in seconds

ht is the heating time in seconds

The time increment, Δt, was restricted to 2.5×10^{-4} seconds to ensure numerical stability, which itself corresponds to a measure of the characteristic time needed for the thermal diffusion front to propagate through a zone.

The thermal conductivity and specific heat properties of calcite and pyrite vary with temperature (Harrison 1997) and have been included as reference in Tables 1 and 2.

Thermal/mechanical Coupling

Stage 3 Thermally generated strains and stresses

At the end of the heating interval the thermally induced strains within a zone, assuming perfect restrainment by the surrounding zones and isotropic expansion is given by Equation 8.

$$\varepsilon_{(i,j)} = -\alpha_{(i,j)}.(Tn_{(i,j)} - T1_{(i,j)}) \qquad (8)$$

Where $\varepsilon_{(i,j)}$ is the strain in zone i,j

$\alpha_{(i,j)}$ is the thermal expansion coefficient (1/°K) of zone i,j

$Tn_{(i,j)}$ is the final temperature of zone i,j

$T1_{(i,j)}$ is the initial temperature of zone i,j

The thermal expansion coefficient for pyrite and calcite has also been found to be temperature dependant (Harrison 1997). Table 3 outlines the thermal expansion coefficient at various temperatures for calcite and pyrite as assumed and implemented within the modelling.

The calculated thermally induced stress within a zone can then be determined using Hoek's law for isotropic elastic behaviour (Equation 9).

$$\sigma_{(i,j)} = \frac{\varepsilon_{(i,j)}.E_{(i,j)}}{(1 - 2.\upsilon_{(i,j)})} \qquad (9)$$

Where $\sigma_{(i,j)}$ = isotropic thermally induced stress within zone i,j assuming perfect restrainment

$E_{(i,j)}$ = Young's Modulus of zone i,j

$\upsilon_{(i,j)}$ = Poisson's Ratio of Zone i,j

Redistribution of Thermally Induced Stresses

To obtain a state of static mechanical equilibrium throughout the domain of the material a redistribution of the thermally induced stresses and strains was necessary. To obtain the equilibrium distribution the model was stepped in FLAC's default calculation mode for static mechanical analysis. This default mode performs an explicit time-marching finite difference calculation utilising Newton's law of motion to relate nodal strain rates, velocities and forces (Itasca 1995). The material was assumed to behave as a linear isotropic elastic medium with mechanical properties determined by the Young's Modulus, Poisson's Ratio and density (Table 4).

Stage 4 Modelling of Thermal Damage Associated with Material Failure and Strain Softening

When static equilibrium was obtained, modelling of the brittle fracture, where the stresses exceeded the strength of the material, was undertaken by simulating the constitutive behaviour of the ore body as an elasto-plastic material with plastic strain softening. The strength of the material was approximated as a very strong brittle crystalline limestone with an unconfined compressive strength of 125 MPa and a shear strength related by a linear Mohr-Coulomb strength criterion (Equation 10).

$$\tau = \sigma_n . \tan\phi + c \qquad (10)$$

Where τ is the shear strength

σ_n is the normal stress acting normal to the shear plane

ϕ is the friction angle of the material

c is the cohesive strength of the material

Upon failure the material was assumed to behave as a brittle linear strain softening medium undergoing plastic deformation with a final residual strength being obtained after 1% strain (Table 4).

Stage 5 Simulations of the Unconfined Compressive Strength Tests on the Thermally Damaged Samples

The effect of thermal heating on the unconfined compressive strength and fracture development within the modelled material was predicted by the simulation of the uniaxial compressive strength test on the thermally damaged models (Figure 8).

The simulation was undertaken as a plane strain analysis with the material being considered as continuous in the out of plane direction. The simulation was undertaken by applying a constant velocity to the grid points positioned at the top and base of the model domain whilst the left and right boundaries where unstrained. This is analogous to a displacement controlled uniaxial compressive strength test. To monitor the load-deformation relationship within the samples during testing, history files were generated of the average stress conditions at the top and bottom boundaries. The models were run until approximately 0.2% axial strain of the sample whereupon the models predicted failure strength and some strain softening details of the samples was obtained.

Results of the Numerical Modelling

Microwave heating times

To determine the effect of microwave heating on the strength of the calcite and pyrite ore, numerically modelling was undertaken for an unheated sample and for samples with microwave heating times of 1

second, 5 seconds, 15 seconds and 30 seconds. It was assumed that the samples were treated in a multimode microwave cavity with a power density that varied from $3x10^9$ watts/m^3 at 300 °K to $9x10^9$ watts/m^3 for temperatures greater than 600 °K

Temperature Distributions

The modelled temperature distributions for each of the four time intervals is shown in Figure 9. It can be seen from the Figure that the highest temperatures and temperature gradients were generated where the pyrite particles were clustered. Table 5 summarises the temperature distributions within the modelled samples for each temperature increment.

Due to the length of time required to heat the pyrite particles within the 2.6 kW microwave cavity, conduction of the deposited thermal energy from the pyrite into the surrounding calcite host was predicted to occur. After 30 seconds of microwave heating time the calcite host had been heated to greater than 600°K. This conduction can be seen to reduce the temperature gradient generated within the ore sample and thus reduce the thermally generated stresses within the sample.

Effect of Microwave Heating on the Unconfined Compressive Strength

The effect of the microwave treatment on the unconfined compressive strength of the ore sample has been illustrated in Figure 10 and summarised in Table 5. Figure 11 shows the unconfined compressive strength of the ore material plotted against microwave heating time and indicates that the heating intervals of 1 and 5 seconds had little affect on the unconfined compressive strength of the material. A more noticeable reduction in strength was predicted with microwave heating times of 15 and 30 seconds. This observation may be attributed to the fact that the

rate of heating was insufficient to induce localised thermal gradients of a magnitude that would generate thermal stresses that exceed the strength of the ore material. Thus the modelled reduction in strength of the ore body may be attributed to the differential expansion of the pyrite and calcite material, due to different thermal expansion coefficients, generating stresses that exceed the strength of the sample.

Pattern of Shear Planes

Also of interest was the pattern of the simulated shear planes developed within the modelled samples after the unconfined compressive tests. These patterns have been shown as Figure 12 for the samples with microwave heating times of 1, 5, 15 and 30 seconds. The fracture patterns developed within the microwave heated samples were similar to the fracture patterns displayed by the unheated sample i.e. consisting mainly of continuous shear planes inclined at approximately 25° to the direction of loading.

Effect of Increasing the Microwave Power Density

Power Density and Heating Time Intervals

To assess the effect of increasing the microwave power density on the temperature distribution, unconfined compressive strength and shear plane development within the ore samples a microwave power density of 1 x 10^{11} watts/m^3 was assumed for the pyrite material. This power density was approximately 10 to 15 times greater than the power density generated by using the 2.6 kW 2.45 GHz microwave cavity, although still easily within the range that can be achieved by microwave heating of pyrite in a single mode cavity (Salsman 1995). It is assumed that this power density is achieved by a single mode cavity supplied with microwave energy at a

power level of 15kW at 2.45GHz (at this power this level of power density is easily achievable). The calcite host material was considered to be unheated by the microwave energy. Due to the higher power density much shorter heating times of 0.05, 0.25, 0.5 and 1 second were considered.

Temperature Distributions

The modelled temperature distributions within the ore samples for each of the four time intervals are shown as Figure 13. The Figure illustrates that significantly greater temperatures were generated within the pyrite particles. The shorter heating times compared to the 2.6 kW microwave cavity reduced the degree of thermal conduction, thus reducing the amount of heating of the calcite matrix. This generated temperature gradients of a significantly higher magnitude within the ore samples. The temperatures within the ore samples obtained by the modelling have been summarised in Table 6.

Effect of Microwave Heating on the Unconfined Compressive Strength

The effect of the microwave heating on the unconfined compressive strength of the ore samples is illustrated in Figure 14. Compared to the reduction in strength within the 2.6 kW cavity it can be seen from Figure 15 that that the higher power density generates a considerably larger reduction in strength, with the majority of the strength reduction occurring very quickly (within 0.05 seconds of microwave heating). The results of the modelling have been summarised in Table 6.

Pattern of Shear Planes

The pattern of shear planes developed within the ore samples after the simulated uniaxial compression test, for the 0.05, 0.25, 0.5 and 1 second

heating intervals are shown as Figure 16. The Figure indicates, unlike the unheated and 2.6 kW cavity heated samples, that the shear planes are irregular and concentrated along the grain boundaries between the pyrite and calcite. This may be attributed to the high thermally induced stress that develop along these boundaries due to the rapid localised heating and expansion of the pyrite particles within the relatively unheated calcite matrix.

Discussion

The influence of microwave power density on a theoretical ore has been demonstrated. The numerical simulation has shown very clearly that if the preferential dielectric material can be made to absorb the majority of the applied energy significant reductions in compressive strength can be achieved. To further illustrate this in the context of comminution the extremely well known relationships developed by (Broch and Franklin, 1972 and Bieniawski,1975) were used to calculate the point load index ($Is_{(50)}$) from the modelled UCS data. The equation used was:-

$$I_s(50) = UCS/K \qquad (11)$$

Where $I_s(50)$ = Point load strength corrected to 50mm core.
K = 24
UCS = Uniaxial compressive strength

The results of this analysis are shown in Figures 17 and 18. Figure 17 shows the influence of microwave heating time versus point load index for the lower power density. It can clearly be seen that as microwave exposure time is increased the point load index decreases significantly.

This is also true in Figure 18, which shows microwave heating time versus point load index for the ore exposed to the higher density. As for the UCS tests in Figures 11 and 15 the reductions in point load index are particularly significant at the higher power density with a reduction from 5.25 for non-treated to 1.25 after just 0.2 seconds.

Point load index is of particular interest to the mineral processing engineer because it allows rapid prediction of the relationships between Ecs (Specific comminution Energy KWh/t) and t_{10} (t_{10} is the percentage passing 1/10th of the initial mean particle size) (Bearman et al 1997). The t_{10} can be interpreted as a fineness index with larger values of t_{10} indicating a finer product. However, in practise the value of t_{10} can be used to reconstruct the size distribution of the broken ore. The t_{10} value is related to the specific comminution energy by the following equation (Napier-Munn et al. 1996): -

$$t_{10} = A[1 - e^{(-b.ecs)}] \qquad (12)$$

Where A and b are material specific breakage parameters. A is the theoretical limiting factor of t_{10} and b is the slope of the ECS versus $t_{10\ \mathrm{plot.}}$ Determination of A and b for a specific material can lead to calculation of a specific size distribution for a specific energy input.

It has previously been shown that point load index is intimately related to Mode 1 fracture toughness (Bearman 1999). Bearman showed that

$$K_{Ic} = 0.209 I_{s(50)} \qquad (13)$$

Where

K_{Ic} + Mode 1 Fracture Toughness ($MN/m^{3/2}$)

Mode 1 fracture toughness has also been shown to have highly significant correlation with the breakage parameters A and b (Bearman et al 1997).

It was shown that:

$$b = 2.2465 \times K_{IC}^{-1.6986} \tag{14}$$

$$A.b = 126.96 \times K_{IC}^{-1.8463} \tag{15}$$

Table 7 shows the calculation of the breakage parameters for the theoretical ore exposed to the 2.6kW microwave radiation for times of 0 10 and 30 seconds. Table 8 shows the calculation of breakage parameters for the same ore treated at the higher power density. This data was used in conjunction with Equation 11 to calculate the influence of ECS on t_{10}. Energy inputs of 0, 0.25, 1 and 2.5 kWh/t were used for the calculation. For clarity data is only presented for the non-treated and the most extreme treatment times i.e. 30 seconds and 0.02 seconds. Figure 15 shows the influence of power density on the ECS v t_{10} graph. It can be seen that as power density is increased the slope of the plot increases significantly and the theoretical limiting value of t_{10} is reached for a much lower energy input. Put simply this means that theoretical ore treated at the lower power density produces a much coarser product for a set specific comminution energy input than that treated at the higher power density. If it is assumed that the mass of material heated is 1kg the sample energy input for each case is for 2.6kW treated sample heated for 30 seconds in the multimode cavity:-

$$2.6 \times 0.5/60 \times 1000/1 = 125 \text{ kWh/t}$$

and for the 15kW treated sample heated in the single mode cavity for 0.2 seconds:-

$15 \times 3.33 \times 10^{-3}/60 \times 1000/1 = 0.8325$ kWh/t.

This clearly shows the influence of power density on the comminution of ores.

The purpose of this discussion has been to illustrate the influence of power density (or electric field strength) on the comminution of minerals. It is appreciated that the texture used for the modelling stage is not exactly like a 'real' ore. However, the ore has behaved in a similar manner to real ores previously tested (Kingman et al. 2000). Also the values obtained for the breakage parameter A are similar to those expected for a typical hard rock ore (Napier Munn 1996). It has been shown that increasing the power density the significantly greater stresses are created for much lower energy inputs. This has significant ramifications for the development of microwave assisted comminution flowsheets. It is concluded that the use of high power density cavities makes the microwave treatment of minerals economic, especially when coupled to the additional benefits of thermally assisted comminution.

The references discussed are in Table 9.

The above theoretical discussion, which we are the first to realise has significance, has been followed up with actual trials of short duration, high field strength, standing wave microwaves on rock samples and they do indeed break along crystal boundaries. Cracks have been seen along grain boundaries – which is very encouraging.

What we have realised is that the previous treatment of minerals has used standard multi-mode microwave cavities, similar to those found in conventional microwave ovens. Whilst a multi-mode cavity is mechanically simple, it suffers from poor efficiencies and relatively low

electric field strengths. We have concluded that high electric field strengths are vital to high power absorption and vital to causing cracking/weakening at the grain boundaries. We have concluded that it is not appropriate to "gently" heat the different phases because that allows time for temperature gradients to be smoothed out. What we want is for a large temperature gradient to be created quickly, so as to induce greater strain/stresses at the grain boundaries. This is achieved better by having high power density microwave radiation.

This is achieved best, we believe, by not having standard multi-mode cavities, but rather having single mode cavities. These particularly comprise a metallic enclosure into which a microwave signal of correct electromagnetic field polarisation is introduced, and undergoes multiple reflections. The superposition of the reflected incident waves gives rise to a standing wave pattern that is very well defined in space. The precise knowledge of the electromagnetic field configurations enables a dielectric material of the rock/other material being treated to be placed in the position of maximum electrical field strength, allowing maximum heating ranges to be achieved. Single mode cavities are not as versatile as multi-mode cavities, but we have realised that by going against traditional preferences for multi-mode cavities and using single mode cavities, we can achieve much higher field strengths. Moreover, it is possible to tune a single mode cavity so as to present the maximum field strength area in a position where it is wanted in the treatment process plant.

Indeed, by having very high field strengths, we can heat materials that are traditionally thought to be transparent to microwaves (or they are apparently transparent in ordinary multi-mode cavities).

By having a power density that is much higher than traditionally achieved in multi-mode cavities, we achieve, very quickly, much higher thermal gradients across grain boundaries than previously achieved.

We have observed in trials 50%, and even 60% changes in strength with exposure times of less that 0.1 seconds. We have proved the principle that it is not necessary to have tens of seconds of exposure to microwaves to get what is wanted.

Figure 3A illustrates a single-mode microwave cavity 30. In this example it is suitable for processing minerals. Minerals, schematically illustrated at 32, enter a microwave pre-treatment zone 34 via an input channel 36. In the example shown in Figure 3, the arrangement is vertical, and the mineral lumps/pieces 32 (which may typically be up to about 15 cm in maximum dimension) fall under gravity through the input channel 36, through the pre-treatment zone 34, and out beyond it through an exit channel 38. The arrangement can be vertical, or inclined to the vertical (for slower feed rate of minerals), or even horizontal.

A microwave emitter 40 is provided in a microwave chamber 42, with the flow of minerals 32 passing through the microwave chamber 42, passing through the pre-treatment zone 34.

A reflector, or microwave short-circuit tuner, 44 is provided disposed opposite to the microwave emitter 40. Another reflector 46 is provided at the microwave emitter 40 (this reflector 46 may be optional). Microwave reflecting surfaces 48 also line the chamber 42.

Microwave emitter 40 emits microwaves, schematically illustrated as 49a, typically of 2.45GHz, or 915MHz (typically available microwave magnetron frequencies). It may emit them continuously, or in pulsed

mode. The microwaves are reflected back from reflector 44 and the reflected waves, schematically illustrated as 49b interfere with the forward waves emitted by the emitter 40 and set up a standing wave pattern. This standing wave pattern has at least one maxima 52 (area where the power density is at a maximum) and minima (areas where the power density is at a minimum).

Because maximum electric field strength is desired, so as to achieve the fastest rate of heating of different materials and hence the fastest differential heating, we ensure that the maxima 52 is at the place where the minerals 32 pass through the pre-treatment zone 34. Alternatively, put another way, we ensure that the materials 32 pass through the treatment zone 34 at a place where the field strength is highest/high enough. We can control either, or both, of where the maxima occur, and where the material is disposed in the cavity. There may be only one maximum in the standing wave.

We have a microwave generating device, and apply microwave energy through a waveguide to a cavity, and couple and tune the cavity to the microwave generating device (magnetron) to maximise electric field strength in the area where the material to be treated is to be found in the cavity.

Figure 3B shows how the electric field strength experienced in the cavity varies across the region of the cavity that is registered with the entrance channel 36. As will be seen, the electric field strength is higher towards the middle cavity/aligned with the middle channel 36, than at the edges. This is due to constructive interference in the standing wave that has been set up.

Figure 4a shows an embodiment similar to Figure 3, but where the input channel 36' directs materials being input into the treatment zone 34' specifically to a place where the standing wave of microwaves has a maxima 52'. In the example of Figure 4a, the mechanism for directing the flowing material through the position of maximum field of strength is a funnel-shaped channel which has an outlet adjacent the maxima 52'. Existing microwave machines can produce only one standing wave, with a single maxima. This may or may not be true in the future.

Figure 4a also shows, conceptually, the ability to tune the standing wave in the cavity/treatment zone 34' to control the position of the maxima. This is schematically shown by having reflector plate 44' be movable relative to the source of the microwaves 40'. The movable nature is shown by dotted alternative positions for the reflector 44', and arrow 56, which illustrates movement of the reflector.

Figure 4b is also relatively fanciful at present (since it is not known how to produce a standing wave as shown) but it schematically illustrates an alternative arrangement were the input channel 36" has a number of guide formations 58, which divide flowable material flowing through the treatment zone into different streams, referenced 60, each of which encounters a different maxima 52" of the standing wave set up in the microwave cavity. It will be appreciated that it is possible to do this by having funnels whose outlets correspond with maxima of the standing wave. If it were possible to have a plurality of maxima then we could do as suggested. That may be available in the future.

The power of the microwave emitter is between 1 and 100 kW, in this example it is15kW. The power density of the microwave emitter is between 10^9 watts per cubic metre and 10^{15} watts per cubic metre. It may be possible to go higher that 10^9 watts per cubic metre in power density,

but there is a potential for higher power densities to cause electric field breakdown of air within the material, which may be detrimental (or which may not be detrimental).

We may prefer to have the size of the "lumps" passing through the treatment chamber to be not too large (for example less than 20cm or less than 15cm in largest dimension).

Figure 2 shows a comminution plant 100 having an ore sizing mechanism 102 which is adapted to ensure that ore leaving the sizing mechanism is of a predetermined maximum size, or range of sizes; a microwave pre-treatment/weakening unit 104 which comprises a unit such as that of Figure 3 or Figure 4a or Figure 4b; a rod mill 106, a first ball mill 108, a first hydrocyclone 110, a second ball mill 112, and a second hydrocyclone 114.

It will be appreciated that items 106 to 114 are prior art, and that the key differentiation from the prior art is the microwave treatment unit 104. However, it will be noted that microwave treatment unit 104 is a weakening unit, and that mechanical comminution is still performed after weakening the ore. It will be noted that it may be necessary, or perhaps not necessary, to mechanically condition/size the ore before it is microwaved in the unit 104. There can be many variations on the comminution circuit of Figure 2.

It is desired to achieve a temperature gradient of between 100 and 1500°C across the grain boundary of a material of the first phase and the material of the second phase, so as to try to induce weaknesses/cracks at the grain boundary.

We realise that the change in strength of the material is a function of power density, that the temperature gradient is a function of power density, that the shear strain is a function of temperature profile, that the shear stress is a function of the shear strain, and that failure will occur when the shear strain in the material exceeds the shear strength of the material. Thus, failure/weakening of the material is intimately associated with power density (obviously assuming that the material contains a mixture of different materials with different dielectric properties). One of the materials must be responsive to microwaves.

It is also a very strong advantage of the present invention that it is a continuous process rather than a batch process. By having a continuous flow of material through a treatment zone, we make the process far more amenable to industrial application. The material to be treated in many embodiments of the invention (whether that be to weaken the bond between two phases or for some other treatment purposes) passes through the cavity/standing wave whilst the standing wave exists. There is relative movement between the standing wave/constructive interference, and the material. This is in contrast to batch processes where the material is loaded into a cavity with the microwave power "off", and then microwaves are applied, and then the microwaves are turned off, and then the material removed from the cavity.

Thus the standing wave can be created and a material flowed/moved through the right part of it. In principle the same standing wave may have streams of material (possibly different material) passed through different parts of it so as to expose the different streams to different electric field strength microwaves. Nevertheless, in order to get the most benefit out of any particular microwave generator (e.g. magnetron) one of the streams will go through the maximum field strength region.

The process may be semi-continuous.

A further significant factor is the fact that we have realised that with sufficiently high field strengths to achieve sufficiently high temperature gradients, the material does not have to be exposed to microwaves for very long. Traditionally, the prior art has exposed materials to microwaves for ten seconds or more, sometimes up to many minutes. We believe that it is necessary to expose the material to microwaves, of sufficiently high field strength, for a second or less, and most preferably for less than about half a second, and even more preferably for a time of the order of 0.2 seconds, or perhaps even less. Figure 15 illustrates that 0.2 seconds is an appropriate time when most of the weakening to the material has been achieved. Similarly, Figure 14 shows that the difference in stress achieved between heating times of 0.5 seconds and 0.25 seconds is not very great, especially in comparison to the difference between 0.05 seconds and 0.25 seconds. This again points to about one quarter of a second being a suitable time to apply high-power microwaves for maximum result per unit cost.

Making the pre-treatment of two phase material with microwaves an economic proposition is improved by heating the materials with microwaves for a shorter time (much shorter) than the prior art suggests is to be done.

The short exposure time to microwaves can be achieved in the examples of equipment given by flowing the material through the treatment zone at a high rate (i.e. so that it flows through the high intensity maxima regions in about a quarter of a second or perhaps less). It might flow through in something of the order of a second or less in other examples. This has the double benefit of achieving the most heating effect per unit cost in microwave power, and also increasing throughput of material through the

heating zone – i.e. treating more material per second than was previously thought possible. This double benefit is very interesting. This also makes microwave pre-treatment even more financially feasible.

The invention is applicable to extracting one phase of material from another phase. For example it can be used to extract a liquid from a solid phase.

In one example, we use 15kW microwave applied for about 0.1 seconds. This gives an idea of what is meant by "high electric field", or "high power density".

It is estimated that the comminution process to recover minerals from ores simply using mechanical treatment of the ores, without microwave treatment, uses about 25kW hours per ton of ore. It is estimated that using the present invention, this energy consumption could be reduced by half, or possibly even down to 80 or 90% less energy.

Since 60% to 70% of mineral processing plant costs relate to plant energy consumption, this is a very significant reduction in the cost of producing minerals. Furthermore, by weakening the material to be broken up by the comminution plant, there is less wear on the plant, the process is speeded up, and there is a higher throughput through the mechanical comminution process. Moreover, because the materials are inter-granually broken, it is easier to recover the desired mineral. The ratio of recovery has been determined to be 3 or 4% better than if no microwave pre-treatment is used.

This experimental result of an increase of a few percent in recovery rate is the first time that this has been observed. We subscribe the achievement of this effect to the higher electric field strength microwaves

that are applied, which in turn is due to the use of single-mode microwave cavities (at least in some embodiments).

We may have a resonance time/time for materials to be in the high field strength region of the cavity of the order of 0.1 to 0.01 seconds, or thereabouts. This is a very high throughput compared to the prior art.

Although gravity-fed systems are what are described in relation to Figures 3, 4a and 4b, it is of course envisaged to have other feed mechanisms, such as pressure fed, conveyor belt fed, fluidised particle fed, centrifugal fed, or hopper fed, etc.

The moisture content of the ore may influence the selected power density.

There may be a control processor controlling the tuning of the microwave cavity, and controlling the position of the maxima, or the position of the material in the cavity and controlling, optionally, the relative position of the flow of materials through the cavity and the position of the maxima. There may be a material-sensor providing feedback signals to the control processor to assist this, and/or there may be an electric field probe to assist this, again providing feedback signals to the control processor. Software to ensure that the physical position of the materials is lined up with the physical position of the maximum intensity of microwaves is also envisaged.

There may be flow-rate control means, optionally controlled by the processor, capable of varying the flow rate of material through the microwave cavity.

Particle size may influence the desired flow rate and/or power density. There may be a particle size sensor, or a particle size input mechanism

(e.g. keyboard), for providing information to the control processor relating to the particle size of the materials being microwaved. The control processor may use this information to vary the flow-rate and/or power density.

There may be a controlled atmosphere in the cavity, for example a nitrogen atmosphere or other inert gas atmosphere.

Other uses for the invention include separating two materials in a general sense - for example de-husking nuts (or making it easier to separate two materials).

Moreover, the idea of using a single-mode microwave cavity to achieve rapid heating using a very high field strength applies to things that do not necessarily involve separating materials. For example, drying materials, processing them to cause changes in the nature of the material, food processing.

The concept of creating a standing wave in a microwave cavity and establishing where in the microwave cavity is the maximum electric field strength of the standing wave and ensuring that material to be processed is disposed in the cavity at the position of maximum field strength, can be applied to all sorts of physical processing. For example, rapid heating can cause fluffing of a material, and rapid heating can be useful in chemical processing. High power density, caused by the formation of a standing wave, typically for a short time, is a distinction over the art.

It will be appreciated that the conceptual, schematic, illustrative, waveforms of amplitudes of standing waves shown in the Figures are not binding and are not restrictive. A three dimensional cavity may have a more complex standing wave, typically with only a single maxima where

constructive interference creates a maximum/maximised field strength region, and the material to be processed will be disposed there.

The presence of the material in the cavity may possibly in some circumstances influence where the maxima is found, and so the cavity may need to be tuned for use with a specific material of a specific volume/shape, or flow rate, at a specific expected place in the cavity. Since electric field strength varies with a general square relationship with power density, electric field strength can fall off quite rapidly with distance as one moves away from a position of maximum intensity – relatively careful alignment of the position of the material to be processed and the cavity/standing wave may be desireable.

Table 9

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CLAIMS

1. A method of weakening the bond between a first phase of material and a second phase of material in a multi-phase composite material, the method comprising inducing a high thermal gradient at an interface between the first and second phases by applying microwaves with a power density of at least $10^9 Wm^{-3}$ and creating a standing wave having an area of high electric field strength and positioning the material at or about the area of high electric field strength.

2. A method according to claim 1 in which a single mode microwave cavity is used.

3. A method according to claim 1 or claim 2 in which the material is microwaved in a microwave cavity which has a maximised field strength, at least at the region where the material is disposed.

4. A method according to any preceding claim comprising creating a standing wave of microwaves in a cavity and ensuring that the composite material is disposed in the cavity at a position on or about a maximum intensity of the standing wave.

5. A method according to claim 4 in which guide means guide the composite material to the position of a maxima of the standing wave.

6. A method according to any preceding claim comprising having a power density of the order of $10^{15} Wm^{-3}$ or above.

7. A method according to any one of claims 1 to 6 comprising applying the microwaves to ore or rocks to facilitate the extraction of a substance from the ore or rock.

8. A method according to claim 7 further comprising mechanically stressing the ore or rock to separate the first and second phase materials.

9. A method according to any one of claims 1 to 8 comprising passing the multi-phase composite material through a microwave cavity in a continuous, non-batch, microwave treatment process.

10. A method according to any one of claims 1 to 9 comprising achieving a temperature gradient of at least, or of the order of, 100°C across the interface between the first and second phase materials.

11. A method according to claim 10 comprising inducing a temperature gradient of at least, or of the order of, 500°C, or 1000°C, or 1500°C, across the interface.

12. A method according to any preceding claim comprising applying the microwaves to the composite material for a time of the order of 1 second or less.

13. A method according to claim 12 comprising applying the microwaves to the composite material for a time of the order of a quarter of a second or less.

14. A method according to claim 12 comprising applying the microwaves to the composite material for a time of the order of 0.1, or 0.01 seconds, or less.

15. A method according to any one of claims 12 to 14 comprising passing the composite mixture through the microwave cavity at such a

speed that it experiences the effect of the high power microwaves for a time commensurate with the times specified in claims 12, 13 or 14.

16. A method according to any preceding claim comprising generating microwaves with a power of the order of at least 1kW.

17. A method according to claim 16 comprising generating microwaves at a power of the order of 10kW or above; or of the order of 100kW, or above.

18. A method of weakening the bond between a first phase of material and a second phase of material in a multi-phase composite material comprising applying a high power density of microwaves, or high electric field strength microwaves, to the composite material for an exposure time that is of the order of one second or less.

19. A method according to claim 18 in which the exposure time is of the order of a quarter of a second or less.

20. A method according to claim 18 or claim 19 in which the exposure time is of the order of 0.1 or 0.01 seconds or less.

21. A method according to any one of claims 18 to 20 in which the power density is $10^9 Wm^{-3}$ to $10^{15} Wm^{-3}$, or more.

22. A method according to any one of claims 18 to 21 in which the electric field strength of the microwaves that encounter the material is of the order of 5×10^4 to 5×10^6 Vm^{-1}.

23. Apparatus for weakening the bond between a first phase of material and a second phase of material in a multi-phase composite material

comprising a microwave cavity adapted to apply high power density microwaves to the composite material for an exposure time that is of the order of one second or less.

24. A method of continuous processing of ore or rocks comprising applying high power density microwaves, or high/electric field strength microwaves, on a continuous basis to ore or rocks passing through a microwave cavity to weaken the ore or rocks, and subsequently passing the continuous flow of ore or rocks to a mechanical treatment machine and mechanically breaking up the ore or rocks.

25. A method according to claim 24 in which the microwaves are applied with a power density of at least $10^9 Wm^{-3}$ and a standing wave of microwaves having a maxima is created, typically using a single mode cavity, and the ore or rocks are passed through the maxima.

26. A method according to claim 24 or claim 25 in which the residence time of the ore or rocks in the high field strength microwaves is of the order of a second or less, or a quarter of a second or less, or 0.1 second or less, or 0.01 seconds or less.

27. Apparatus for continuous processing of ore or rocks comprising means for applying high power density microwaves, or high or maximised electric field strength microwaves, on a continuous basis to ore or rocks passing through a microwave cavity to weaken the ore or rocks and feed means adapted to pass subsequently the continuous flow of ore or rocks to a mechanical treatment machine adapted mechanically to break up the ore or rocks.

28. A method of separating a first phase of material from a second phase of material comprising creating a temperature gradient at an

interface between the first and second phases of at least 100°C by using a standing wave of microwaves to heat the first and second phases differentially.

29. Apparatus for separating a first phase of material from a second phase of material, the apparatus being capable of creating a temperature gradient at an interface between the first and second phases of at least 100°C by creating a standing wave of microwaves to heat the first and second phases differentially.

30. Apparatus according to claim 29 in which a single mode cavity is provided to produce the standing wave.

31. A method of rapidly heating a material comprising creating a standing wave of microwaves having a region of maximised electric field strength, and having the material disposed in said region of maximised electric field strength.

32. A method according to claim 31 in which the standing wave is created using a single mode microwave cavity.

FIG. 1A

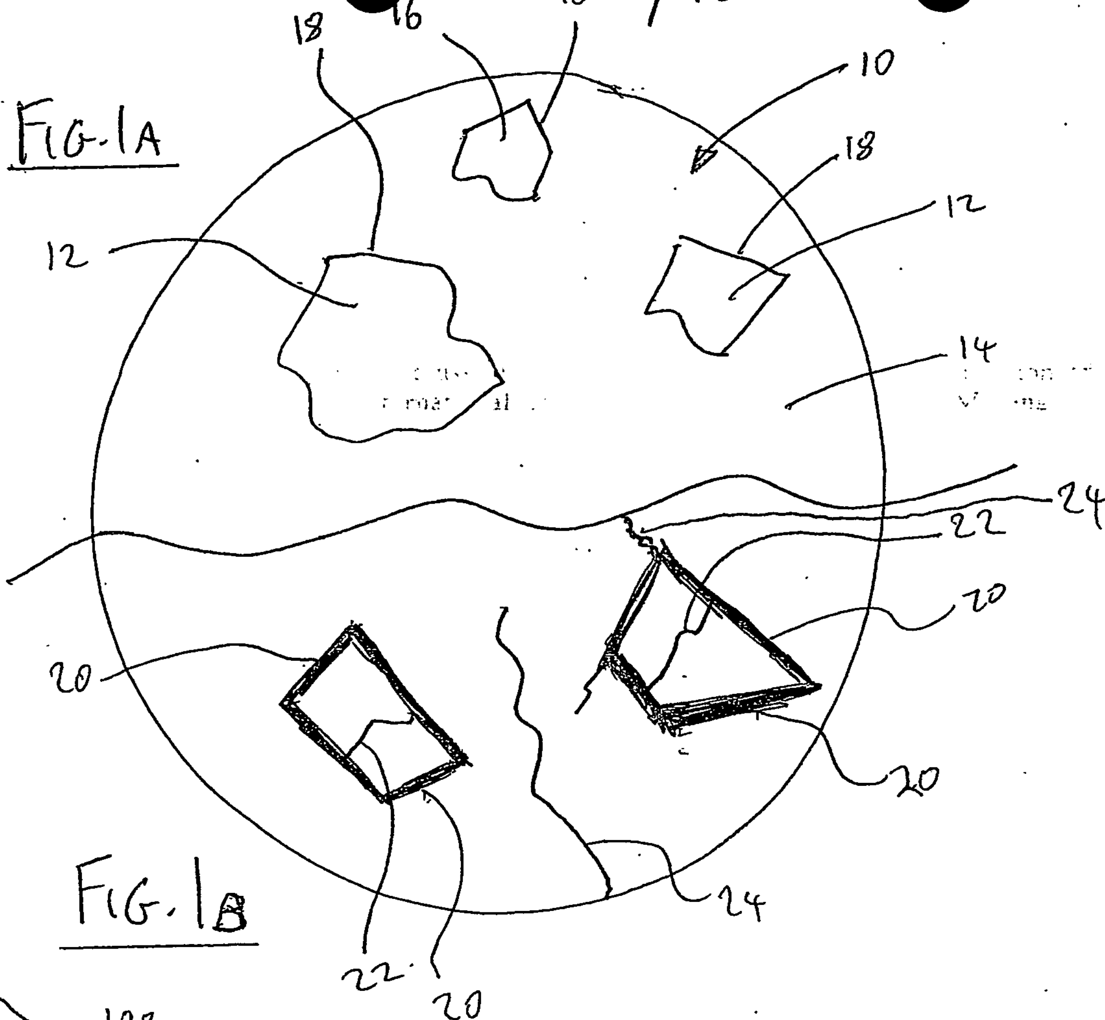


FIG. 1B

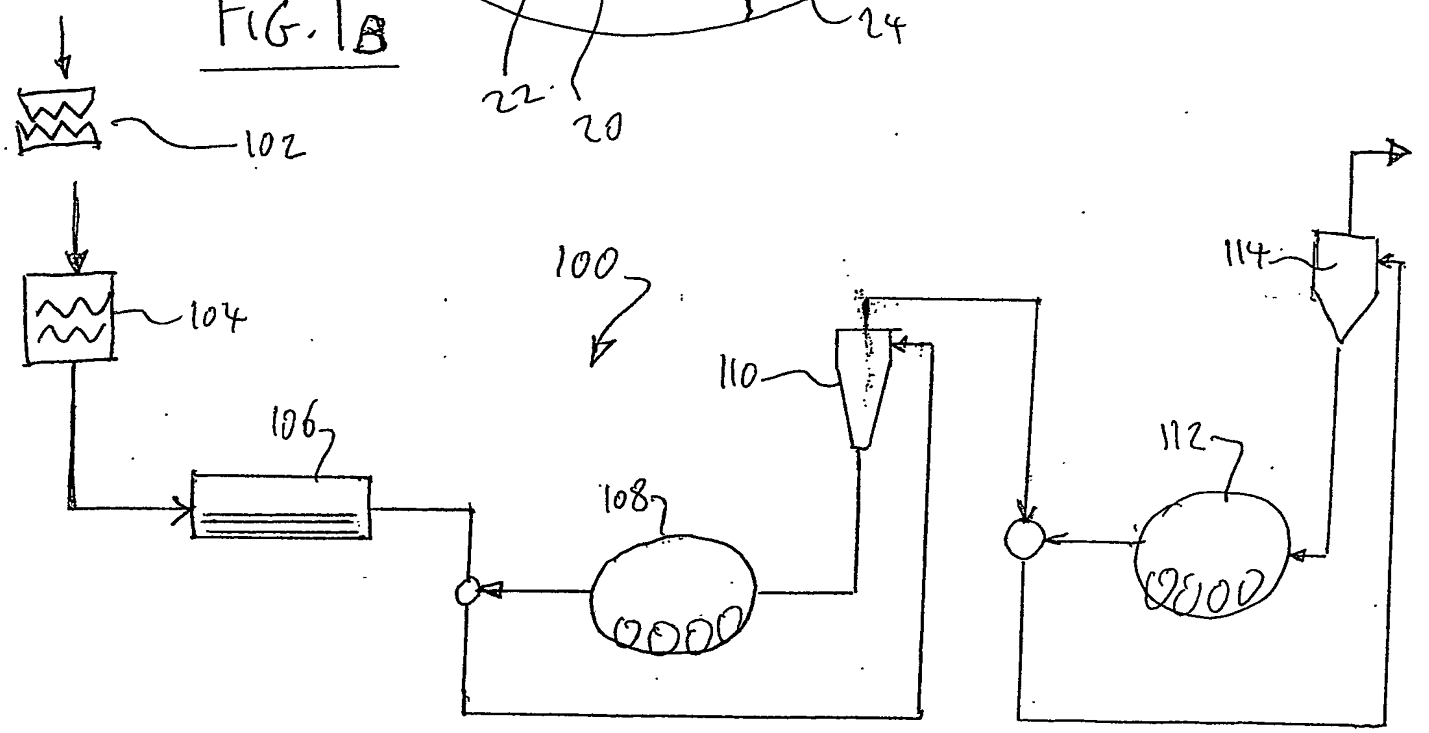


FIG. 2

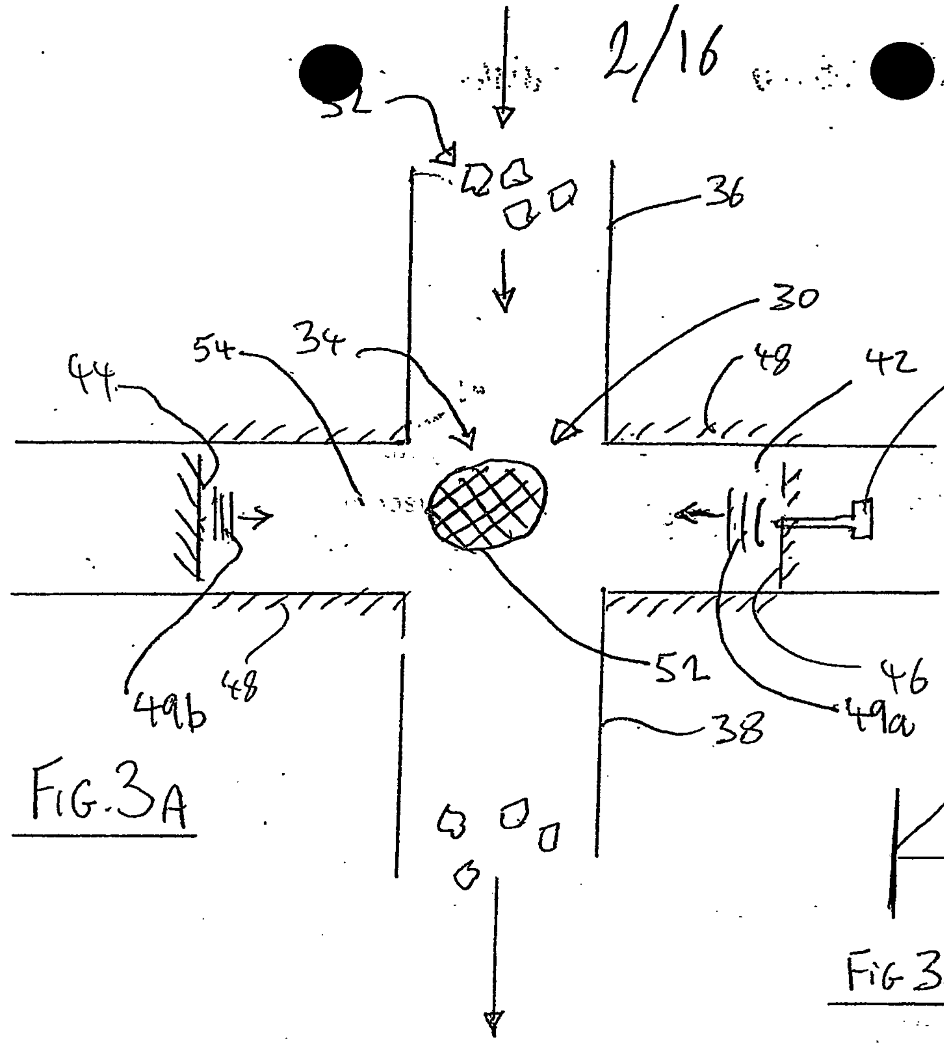


FIG.3A

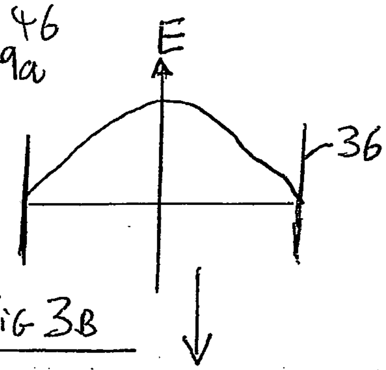


FIG 3B

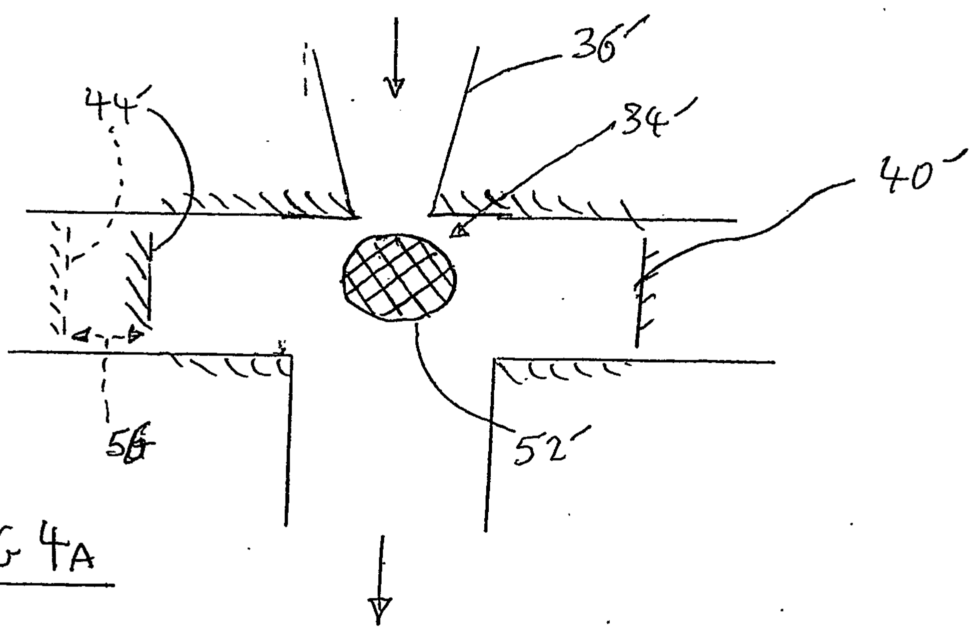
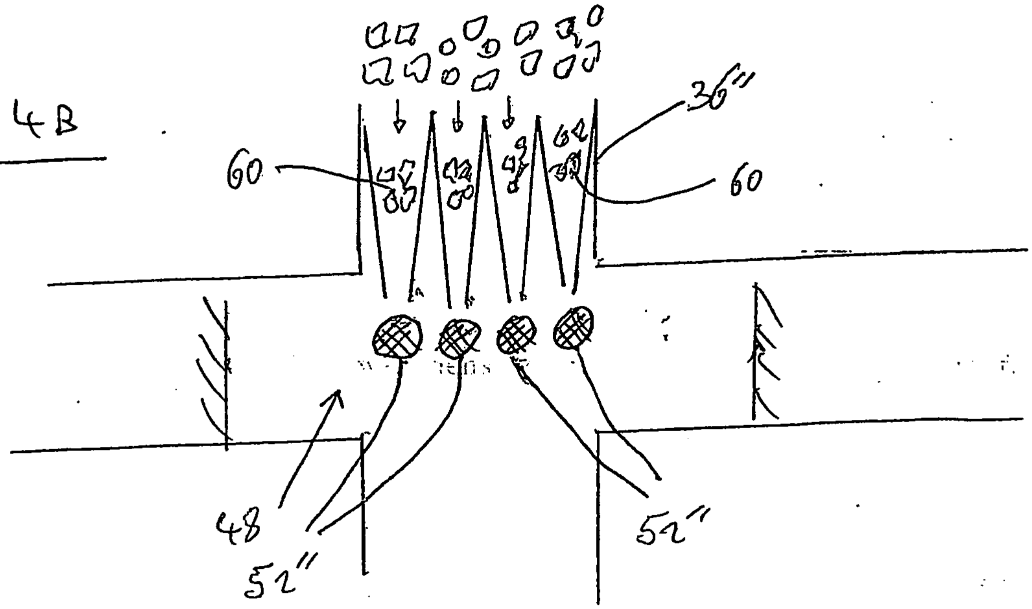


FIG 4A

FIG 4B



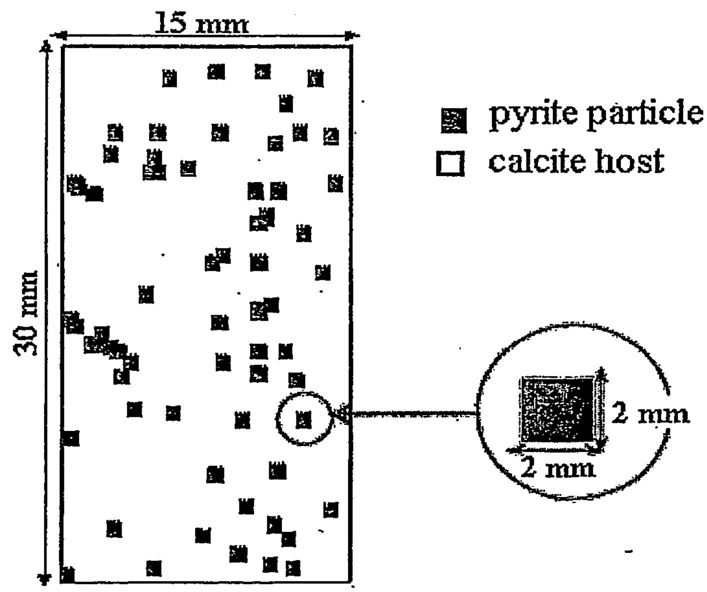


Figure 5 Model of the Calcite and Pyrite Ore Sample

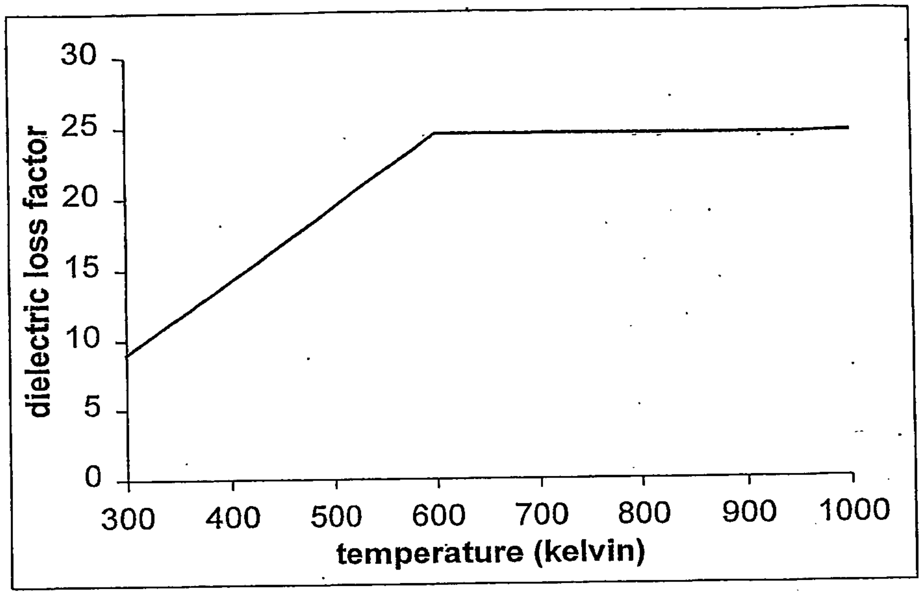


Figure 6 Variation of dielecric loss factor of pyrite as function of temperature

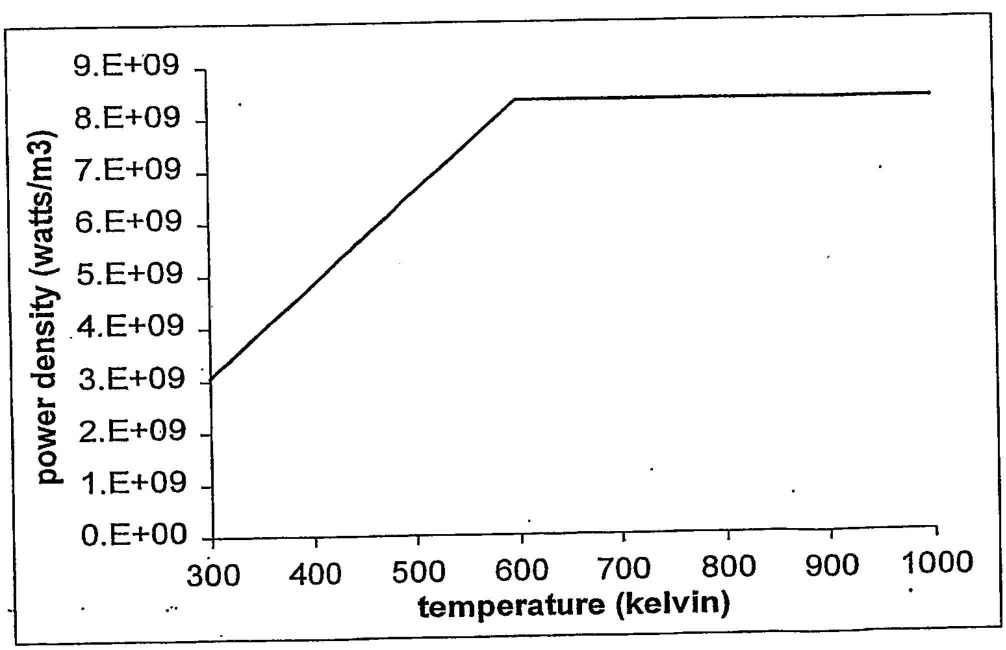


Figure 7 Variation of microwave power density of pyrite in a 2.6kW 2.45 GHz Cavity as a function of temperature.

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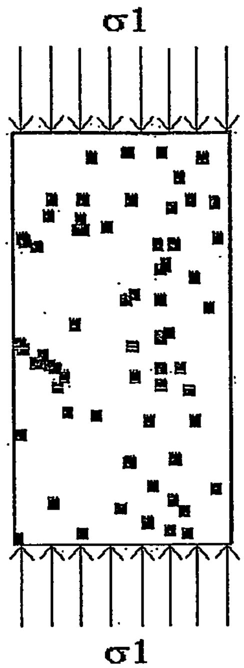

Figure 8 Direction of Simulated Loading During the Modelling of the Uniaxial Compression Test

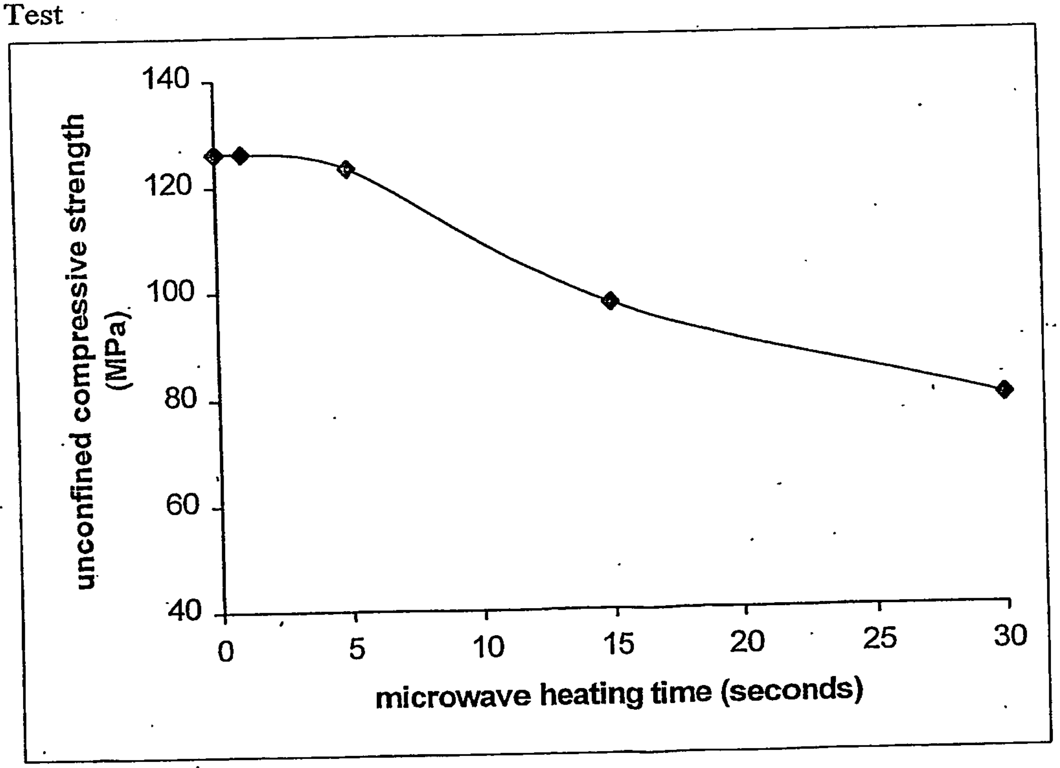

Figure 11 Affect of Microwave Heating time on the Predicted Unconfined Compressive Strength of the Theoretical Calcite and Pyrite Sample (2.6kW 2.45 GHz cavity, power density between $3\times10^9 W/m^3$ and $9\times10^9 w/m^3$)

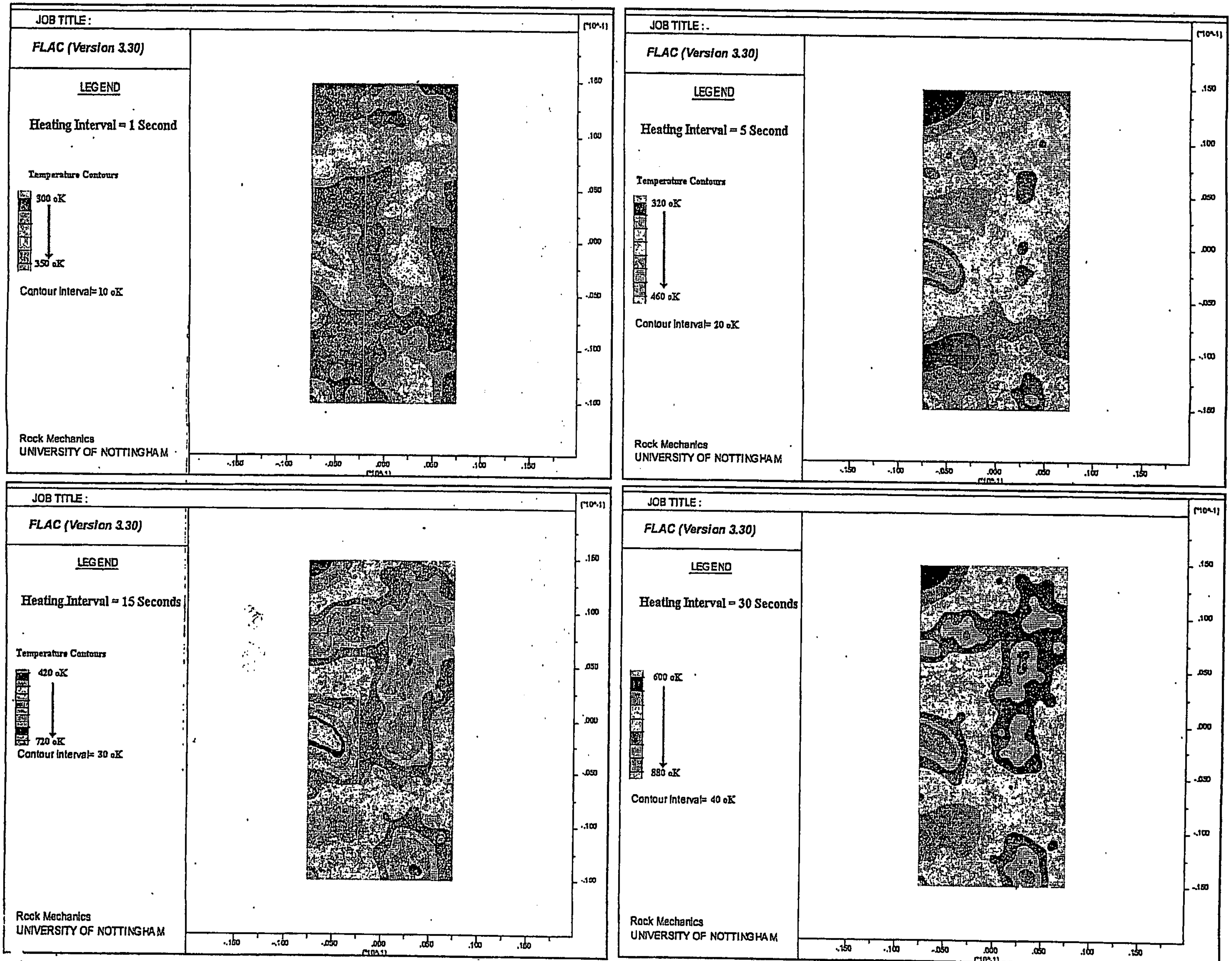

Figure [illegible] Modelled Temperature Distributions for a 2.45 GHz 2.6 kW Microwave Cavity (power density between $3\times10^{9}W/m^{3}$ and $9\times10^{9}w/m^{3}$)

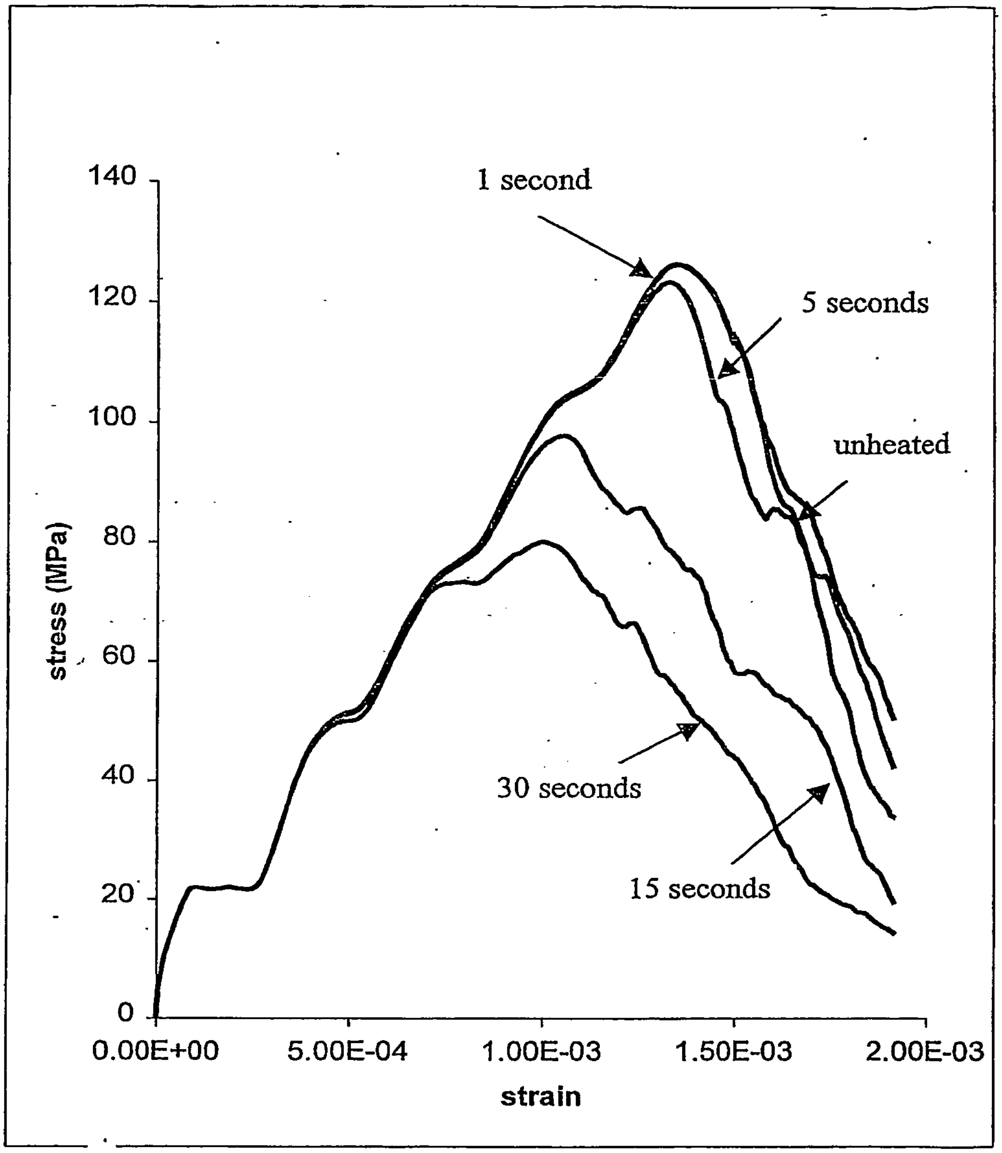

Figure 10 Affect of Varying Heating Times on the Numerically Modelled Stress-Strain Curves for the Theoretical Calcite and Pyrite Sample (Heated in a 2.6 kW 2.45 GHz Microwave Cavity, power density between $3\times10^9 W/m^3$ and $9\times10^9 w/m^3$)

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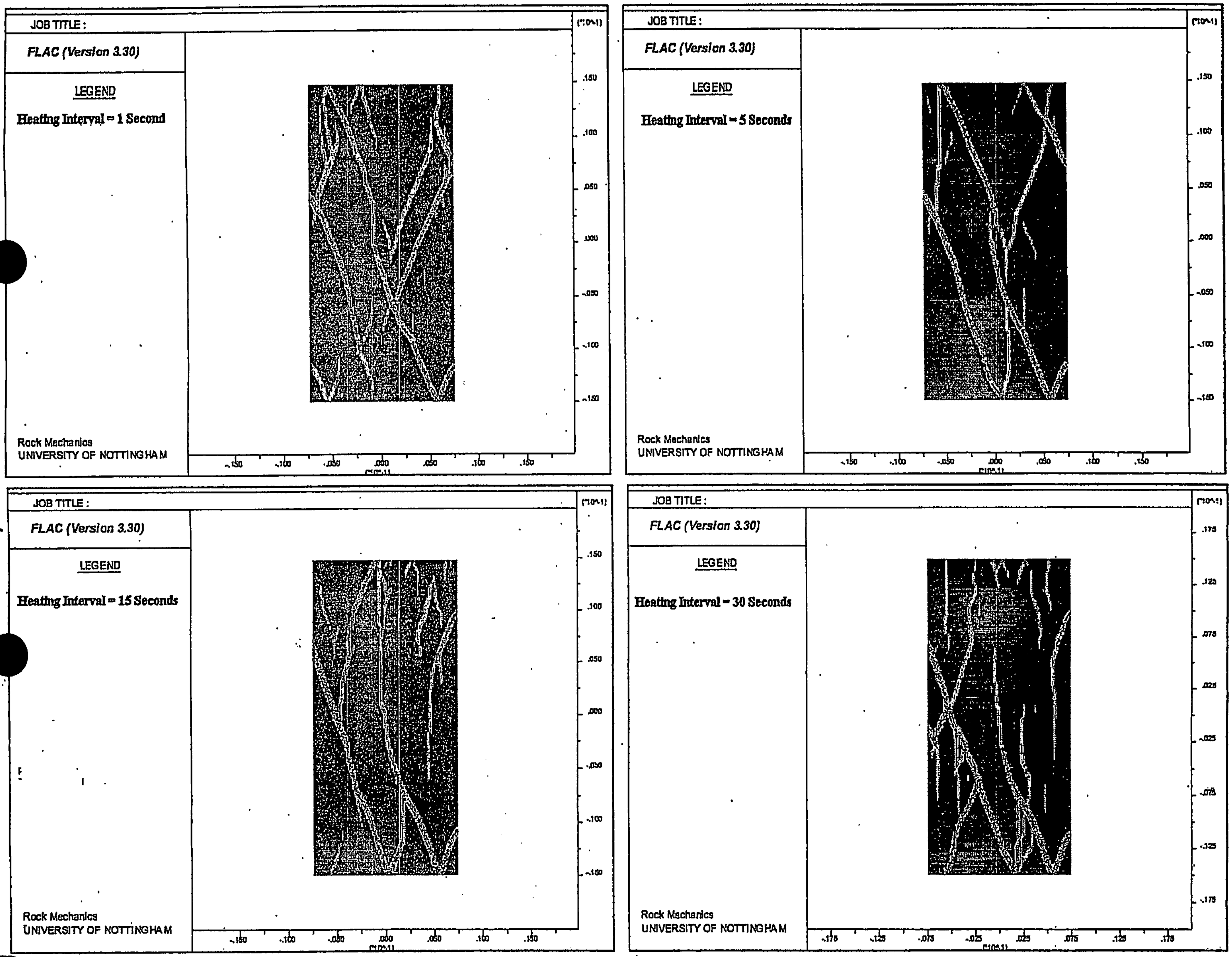

Figure 12 Shear Plane Development During Unconfined Compressive Tests for a 2.45 GHz 2.6 kW e Cavity PD between 3×10^{9} W/m^{3} and 9×10^{9} w/m^{3})

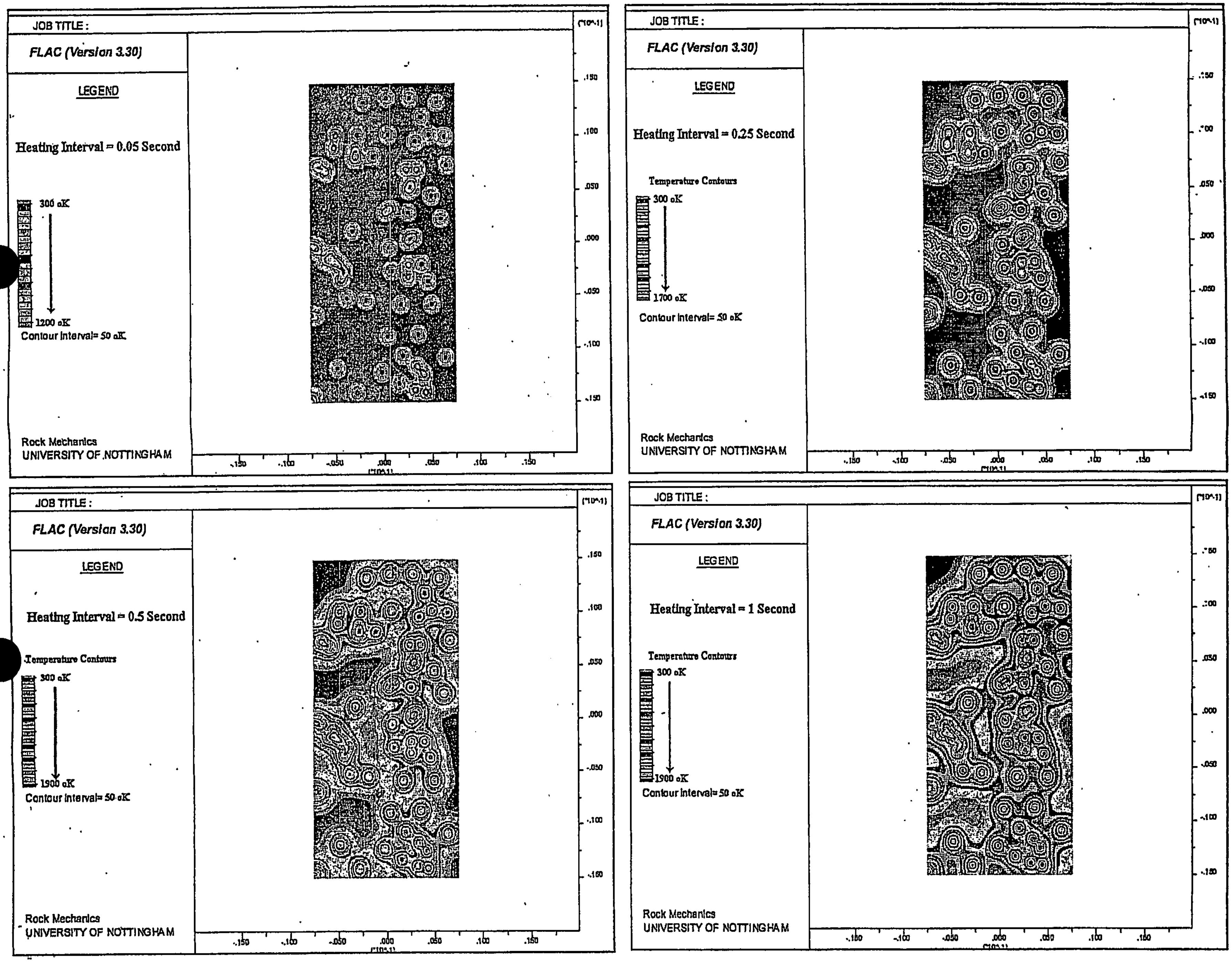

Figure 13 Modelled Temperature Distributions for a Microwave Cavity with a Power Density of $1x10^{11}$ watts/m^3

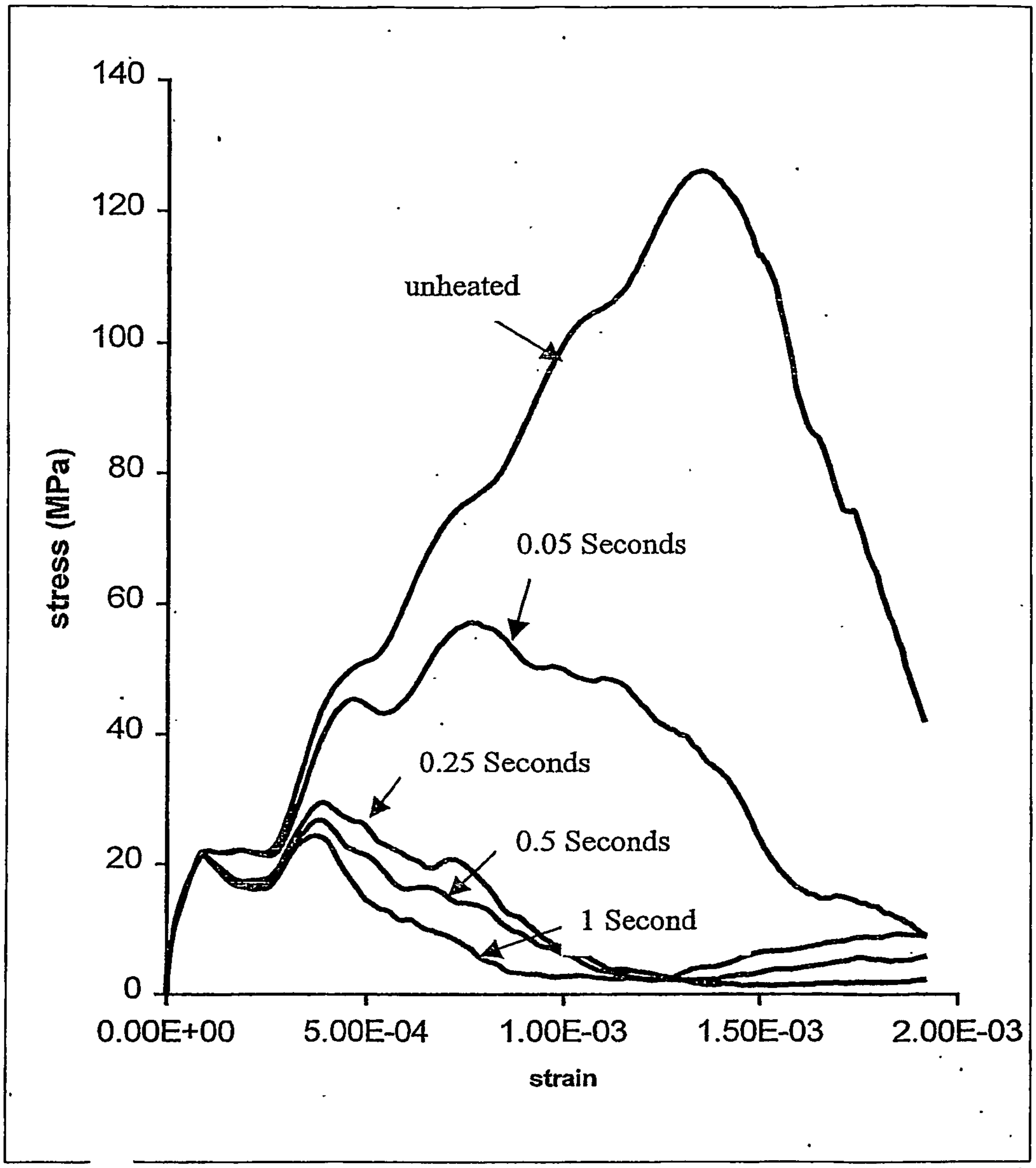

Figure 14 Affect of Varying Heating Times on the Numerically Modelled Stress-Strain Curves for the Theoretical Calcite and Pyrite Sample (Heated Microwave Cavity with a Power Density of $1x10^{11}$ watts/m^3)

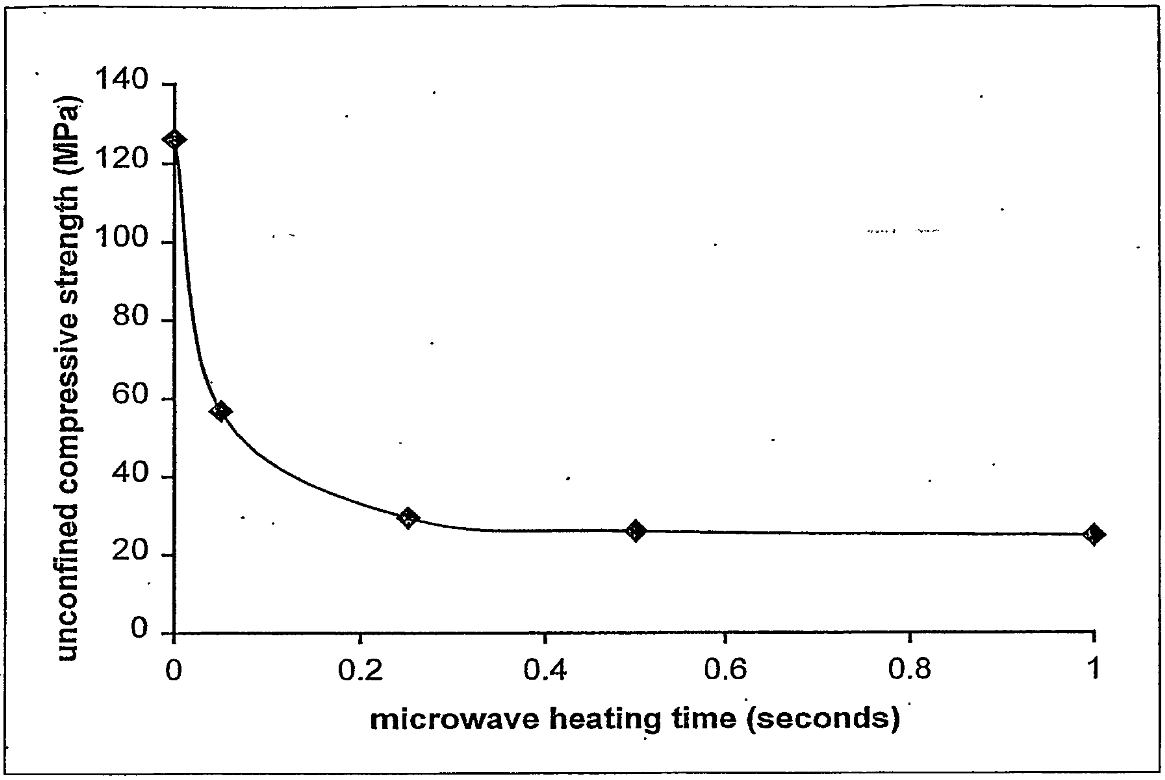

Figure 15 Affect of Microwave Heating Time on the Unconfined Compressive Strength of the Theoretical calcite and Pyrite Sample (power density $1x10^{11}$ watt/m^3)

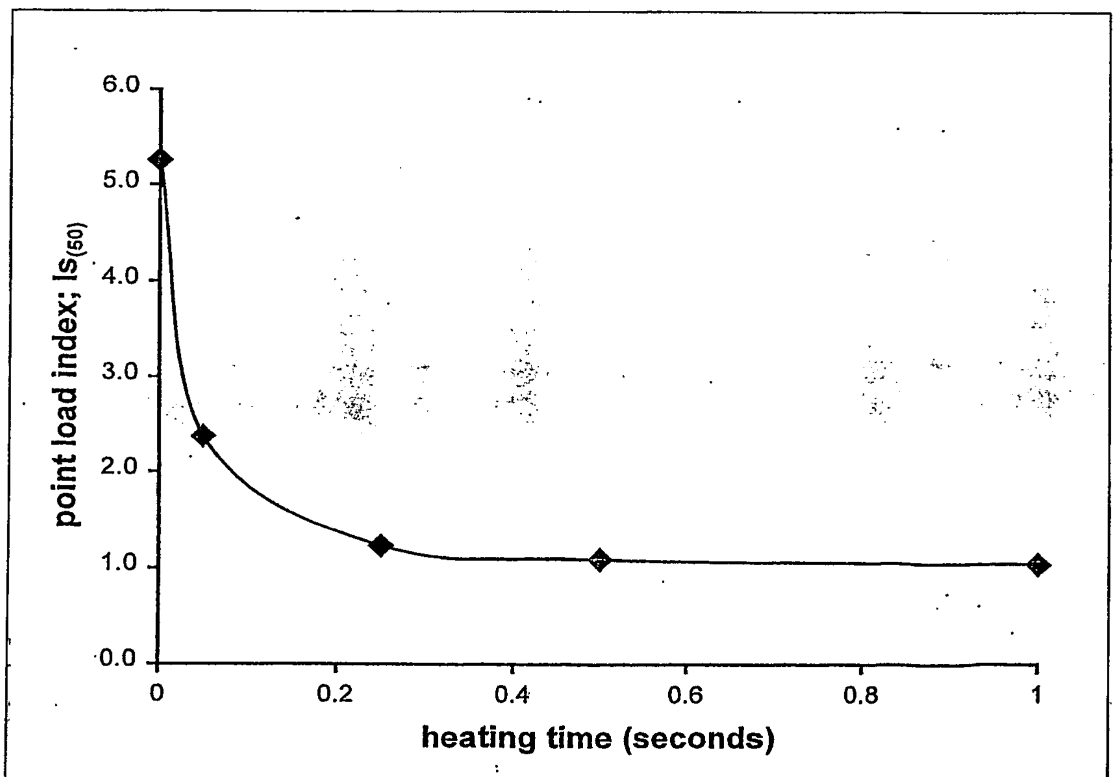

Figure 17 Microwave Heating Time (Power Density =1x 10^{11} watt/m^3) vs Point Load Index

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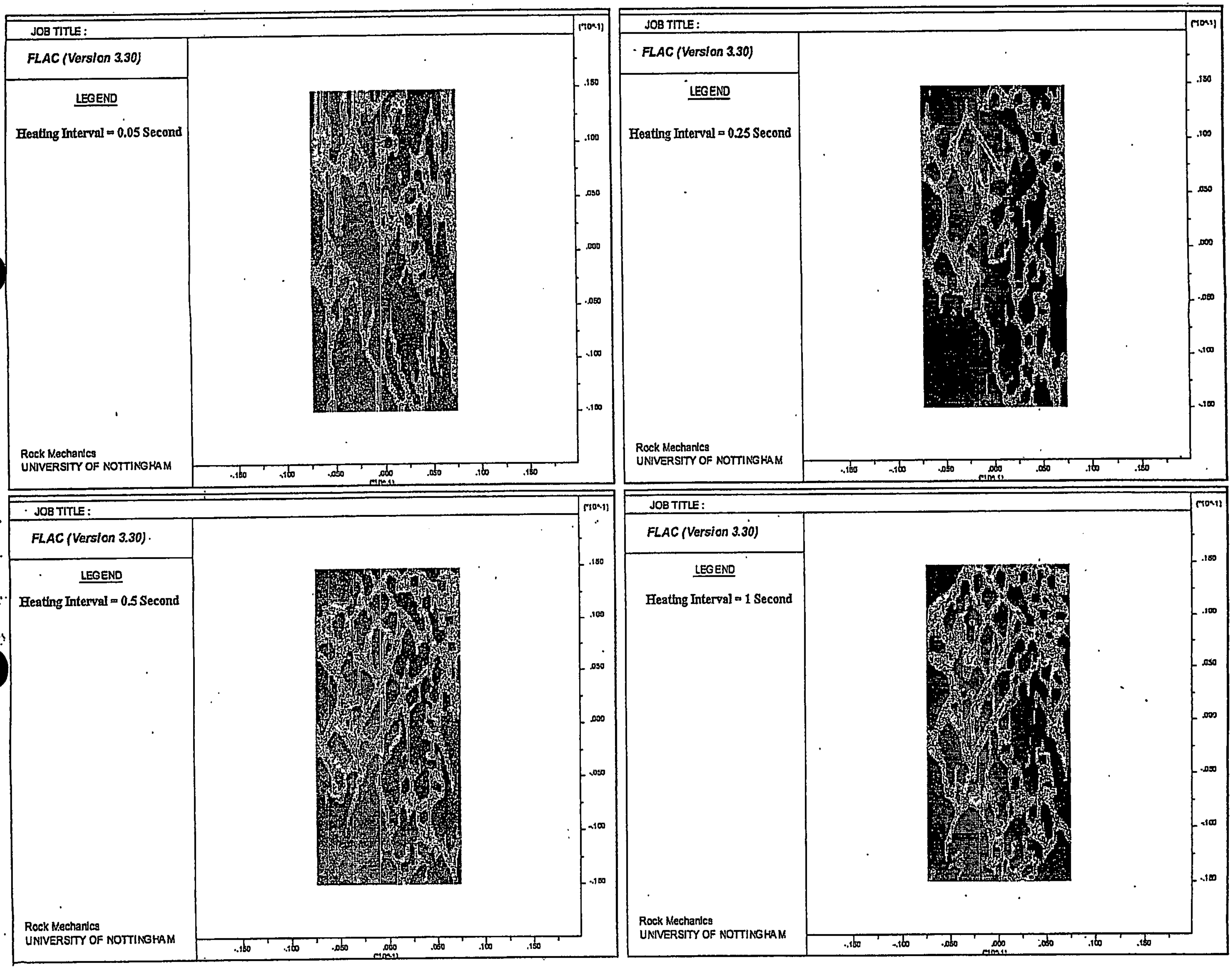

Figure 16. Modelled Shear Plane Development During Unconfined Compressive Tests for a Microwave Cavity with a Power Density of $1x10^{11}$ watts/m^3

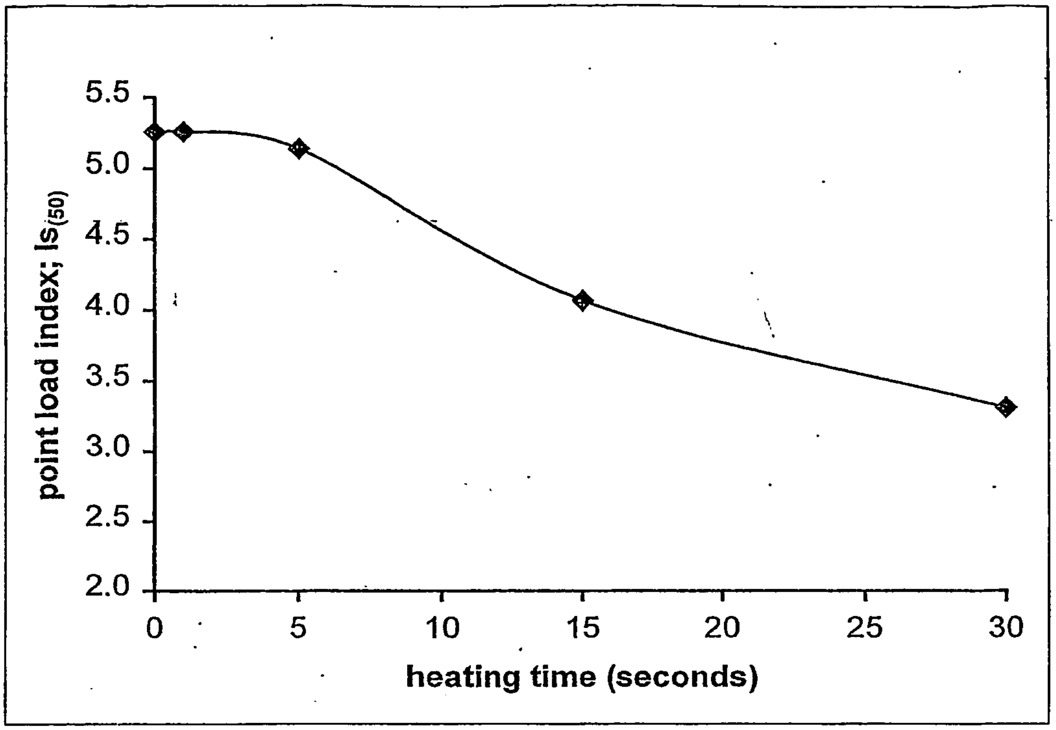

Figure 18 Microwave Heating Time (2.6 kW 2.45 GHz power density between 3×10^9W/m^3 and 9×10^9w/m^3)) vs Point Load Index

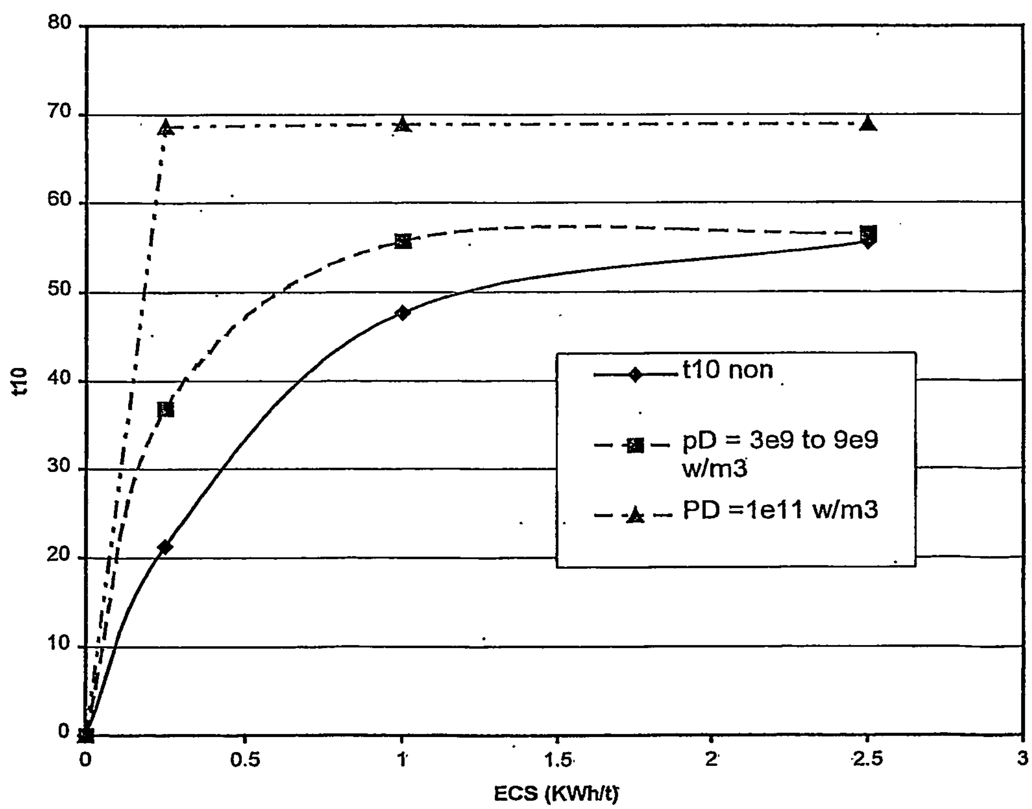

Figure 19. Plot of ECS vs t10 for Non-Treated and Microwaved Samples

Mineral	Specific heat capacity (J/Kg°K)		
	298°K	500°K	1000°K
Calcite	819	1051	1238
Pyrite	517	600	684

Table 1 Specific Heat Capacity as a Function of Temperature

Mineral	Thermal conductivity (W/m°K)		
	273°K	373°K	500°K
Calcite	4.02	3.01	2.55
Pyrite	37.90	20.50	17.00

Table 2 Thermal Conductivity as a Function of Temperature

Mineral	Thermal expansion coefficient (1/°K)			
	373°K	473°K	673°K	873°K
Calcite	13.1×10^{-6}	15.8×10^{-6}	20.1×10^{-6}	24.0×10^{-6}
Pyrite	27.3×10^{-6}	29.3×10^{-6}	33.9×10^{-6}	-

Table 3 Thermal Expansion Coefficient as a Function of Temperature

Mineral	density Kg/m^3	Young's Modulus GPa	Poisson's Ratio	Peak Strength			Residual Strength (after 1% strain)		
				ϕ °	c MPa	T MPa	ϕ_r °	c_r MPa	T_r MPa
Pyrite	5018	292	0.16	54	25	15	54	0.1	0
Calcite	2680	797	0.32	54	25	15	54	0.1	0

Table 4 Mechanical Properties of the Minerals

Heating time (seconds)	Maximum temperature (°K)	Minimum temperature (°K)	Unconfined compressive strength (MPa)
0	300	300	126
1	350	300	126
5	460	320	123
15	700	400	97
30	900	600	79

Table 5 Modelled Temperatures and Unconfined Compressive Strengths for Various Microwave Heating Times (2.6kW 2.45Ghz Microwave Cavity power density between $3\times10^9 W/m^3$ and $9\times10^9 w/m^3$)

Heating time (seconds)	Maximum temperature (oK)	Minimum temperature (oK)	Unconfined compressive strength (MPa)
0	300	300	126
0.05	1200	300	57
0.25	1700	300	29
0.5	1900	300	26
1	1900	300	25

Table 6 Modelled Temperatures and Unconfined Compressive Strengths for Various Microwave Heating Times (Microwave Cavity with a Power Density of $1x10^{11}$ watt/m^3).

time (secs)	Is(50)	Kic	b	A.b	A
0	5.25	1.097	1.91	107.61	56.03
10	4.45	0.93	2.54	145.16	57.14
30	3.4	0.7106	4.22	238.56	56.63

Table 7 Breakage Parameters for 2.6kW Multimode Cavity Microwave Treatment (power density between $3\times10^9 W/m^3$ and $9\times10^9 w/m^3$)

time	Is(50)	Kic	b	A.b	A
0	5.25	1.097	1.91	107.01	56.03
0.1	1.8	0.376	11.83	772.67	65.31
0.2	1.25	0.2615	21.96	1513.41	68.91

Table 8 Breakage Parameters for 15kW, 2.45GHz (Power density 1×10^{11} w/m ^{3} Single Mode Microwave Cavity Treated Ore